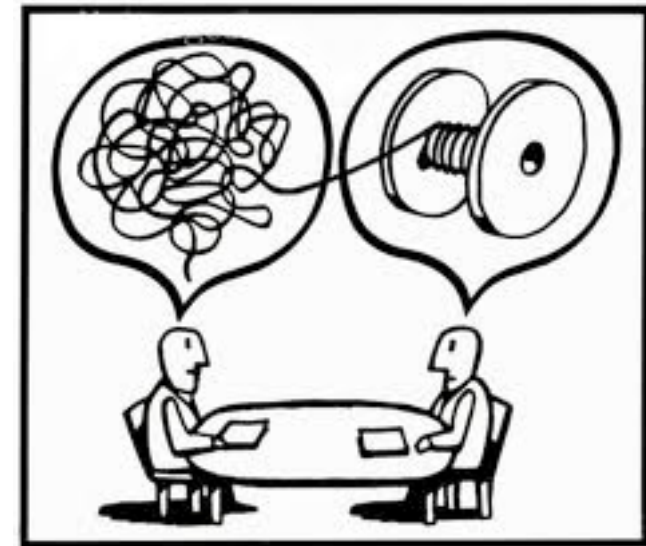


The Physics and Technology of RF Heating and Current Drive in Fusion Plasmas

J.-M. Noterdaeme

with input from
many colleagues

International ITER School
Ahmedabad, December 2012



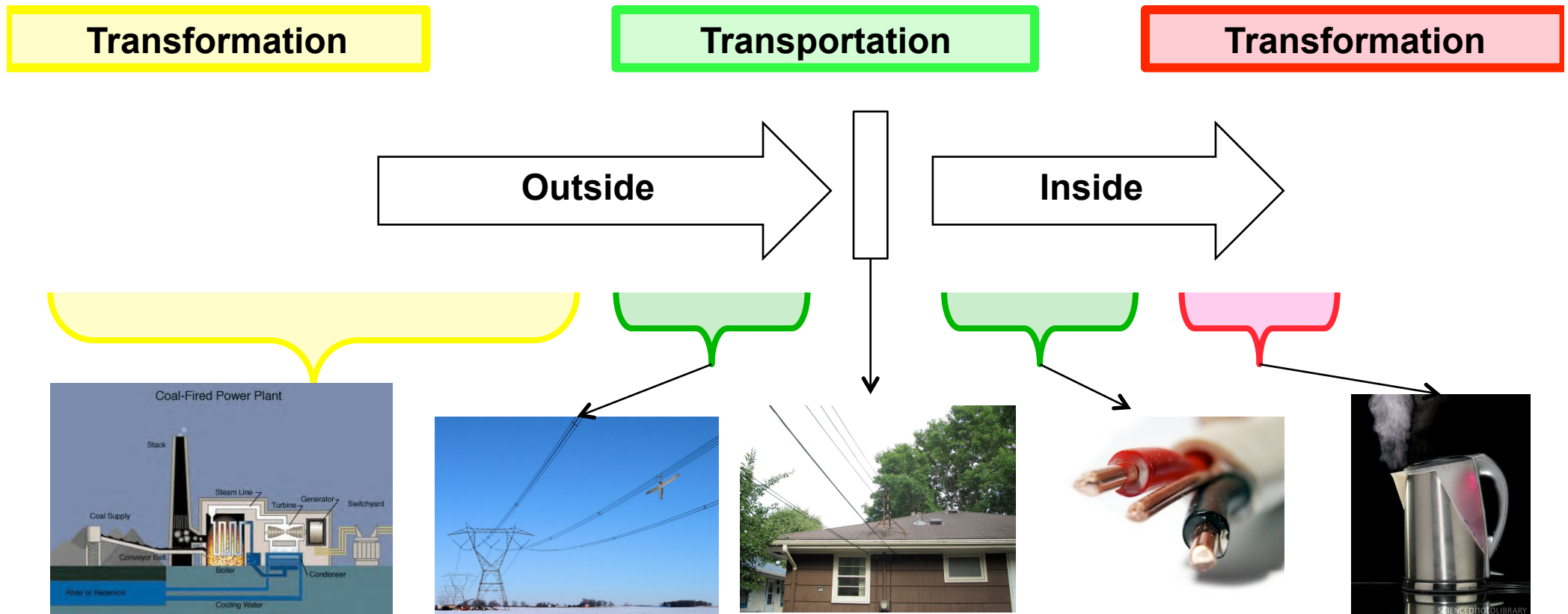
Why?

**Why do we use those heating and current drive methods
we use?**

Because only for those are we able to:

- 1. Generate the power: transformation**
- 2. Transport it to the plasma**
- 3. Transport it inside of the plasma**
- 4. Have it absorbed inside of the plasma: transformation**

Requirements, an example



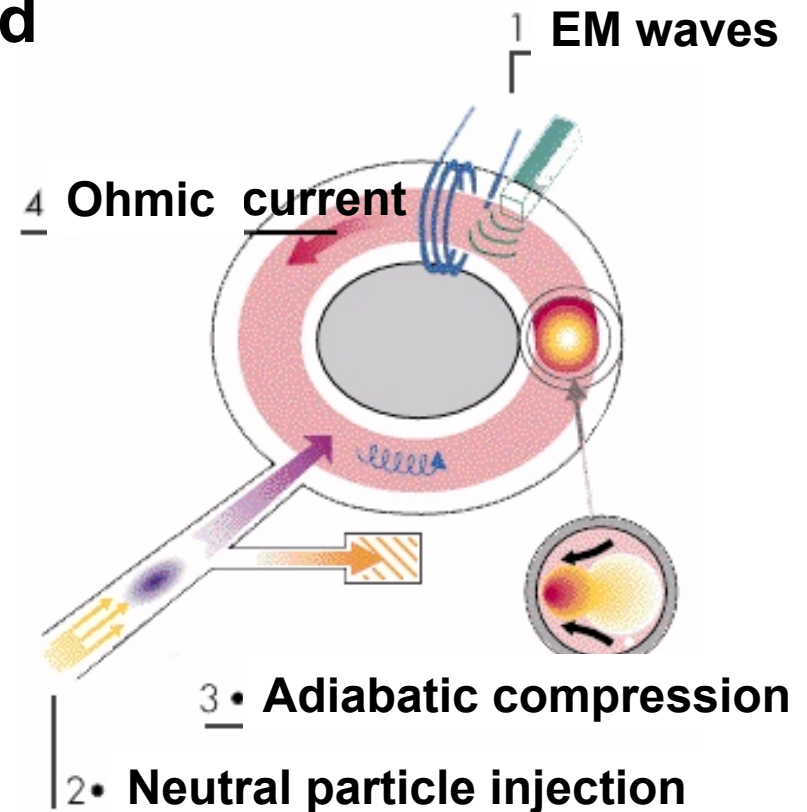
Possible Heating methods

depend on the confinement method

- Ohmic current
- Compression
- Neutral beam injection
- EM Wave (EC, LH, IC, ...)

- Laser beam
- Charged particle beam
- Kinetic energy
- Magnetic energy

- Self-heating (alpha particles)



Particles
Electromagnetic

Other uses of the “heating” methods



- **“Heating” methods, but not just for heating**

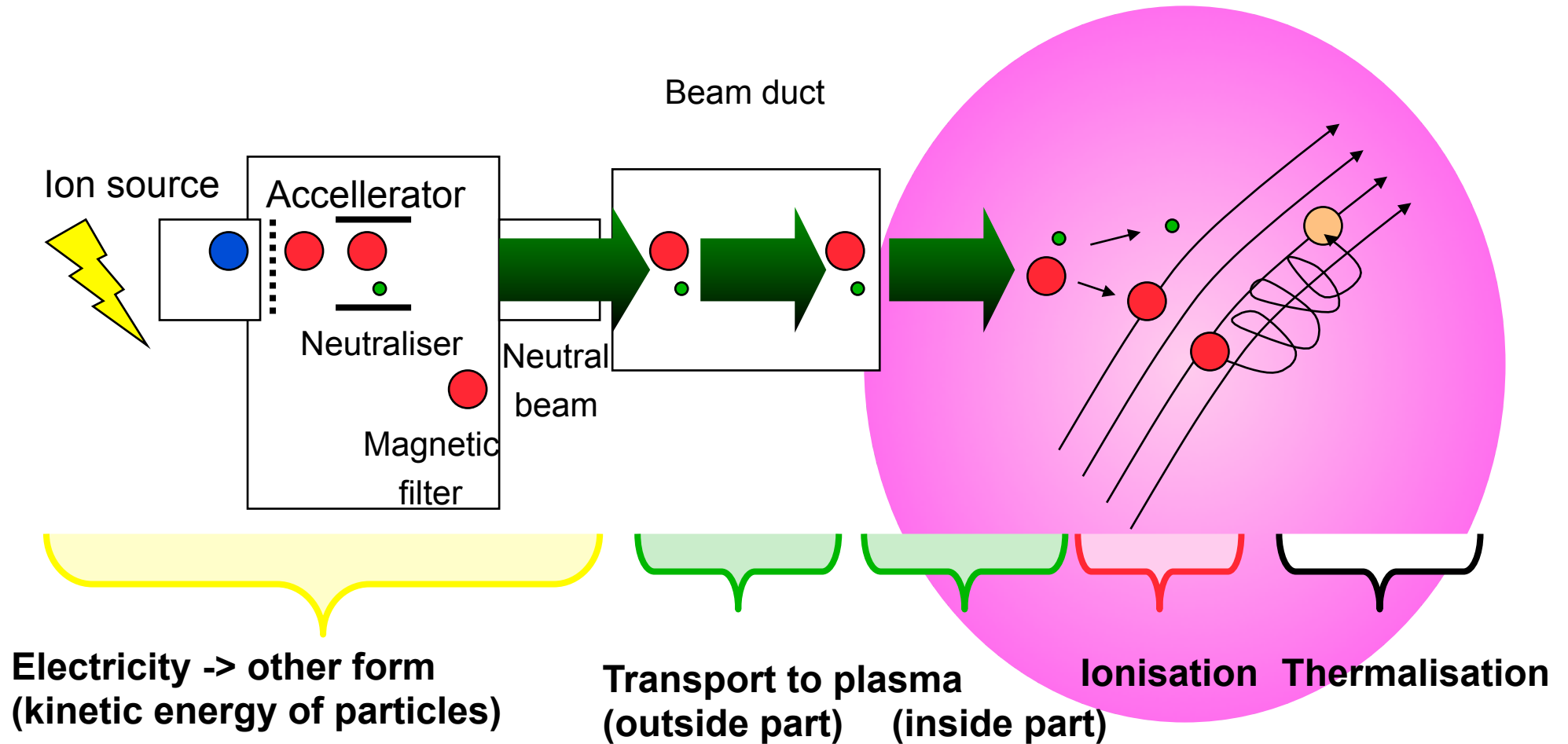
and current drive

- Bulk current
- Localised current

- **Depending on the method, also used for**

- Control
- Fuelling
- Inducing Rotation
- Transport of fast particles
- Diagnostics

Neutral Beam Injection: principle



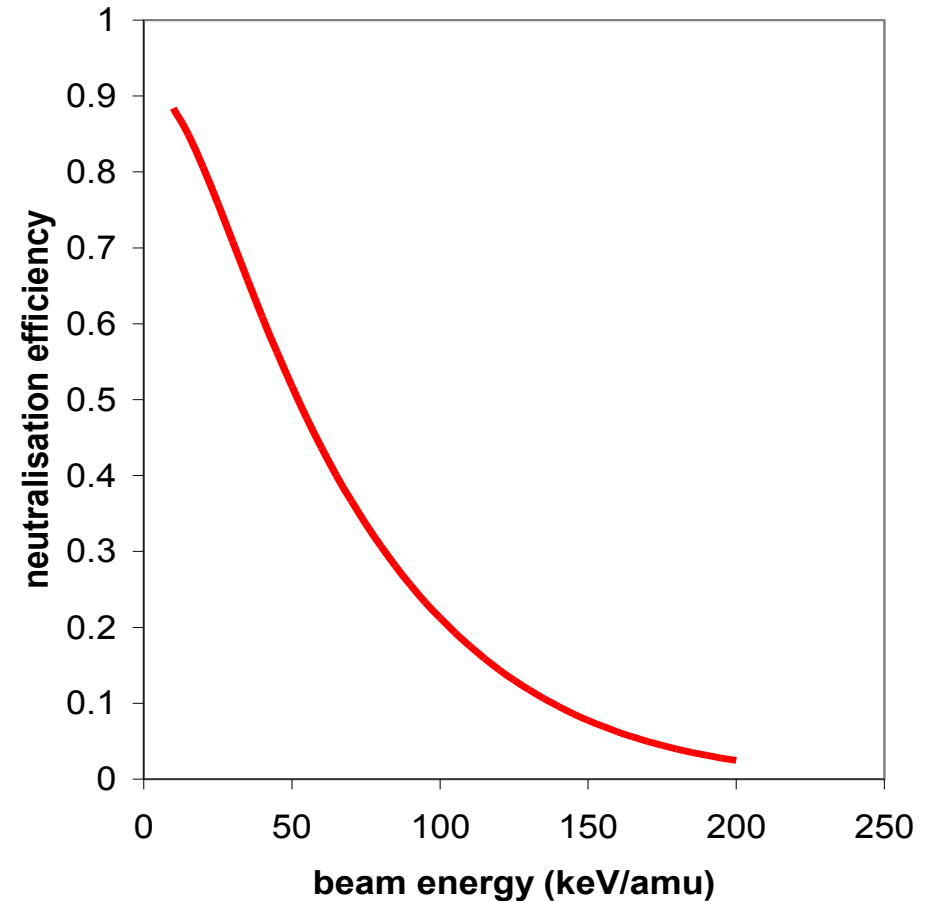
Problem: transport in the plasma

- Neutrals get easily ionized

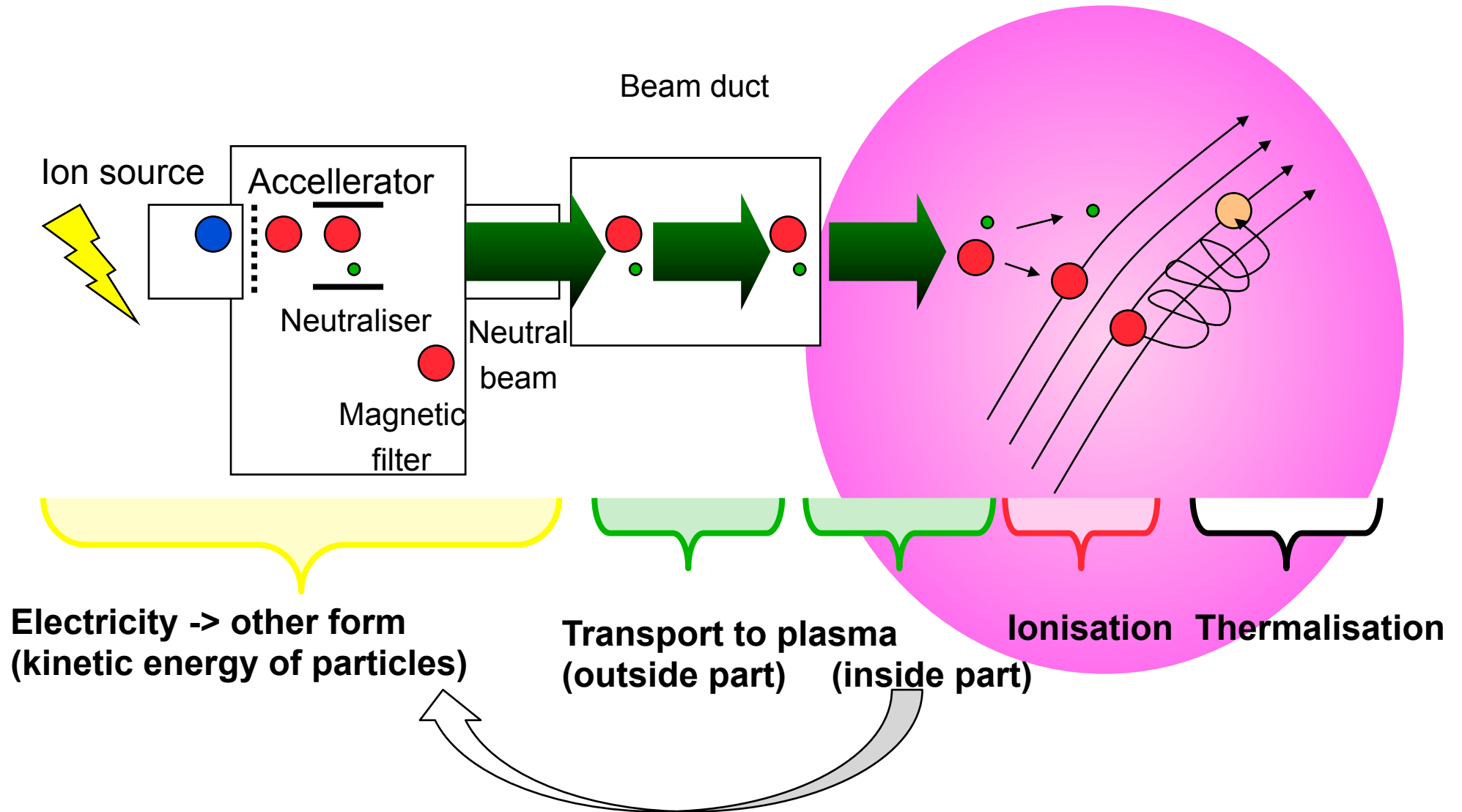
Therefore large machines
need high beam velocities
thus high beam energies

- Energetic positive ions
are difficult to neutralise

Positive Ion Neutralisation Efficiency H^+ on H_2

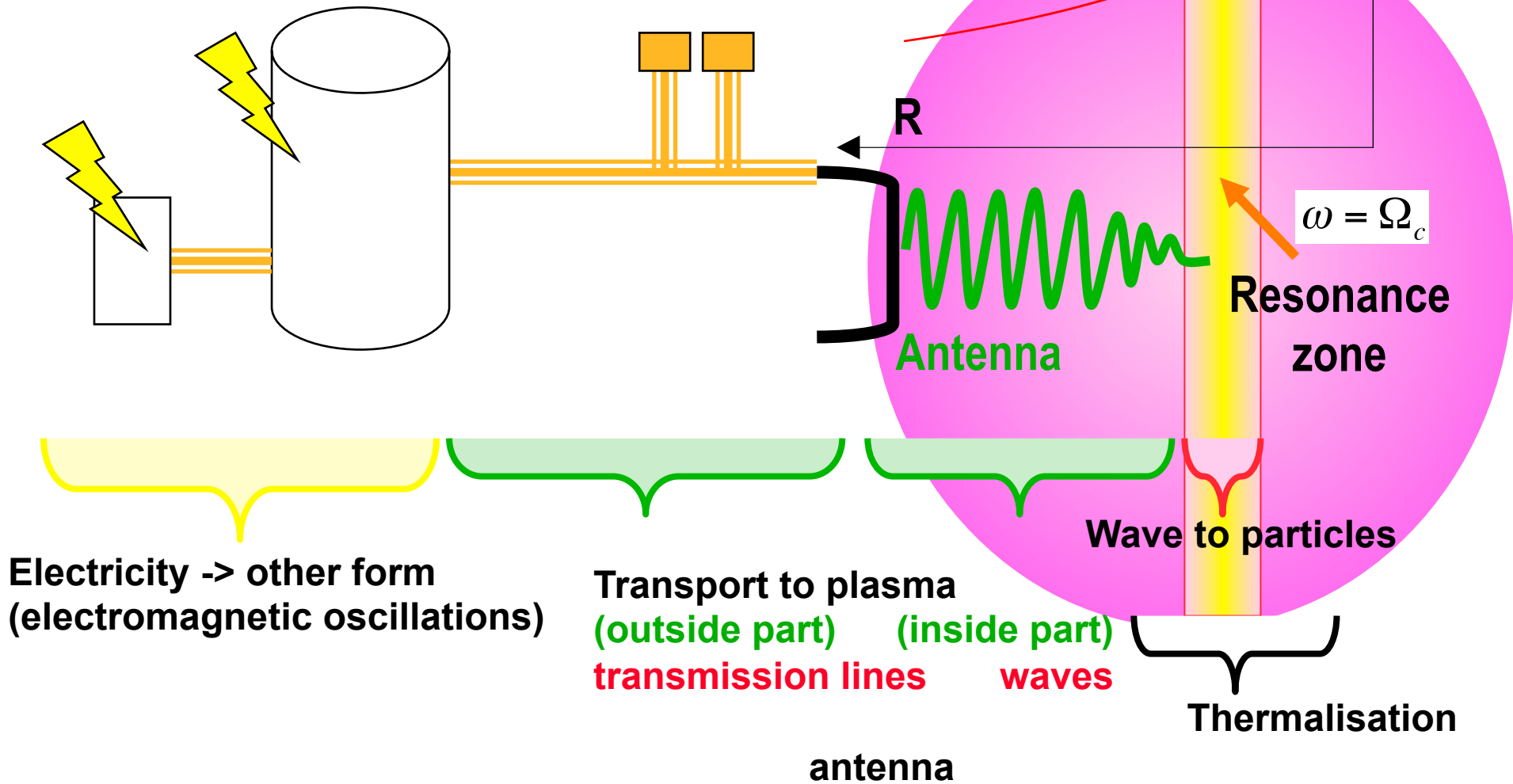


Neutral Beam Injection: principle



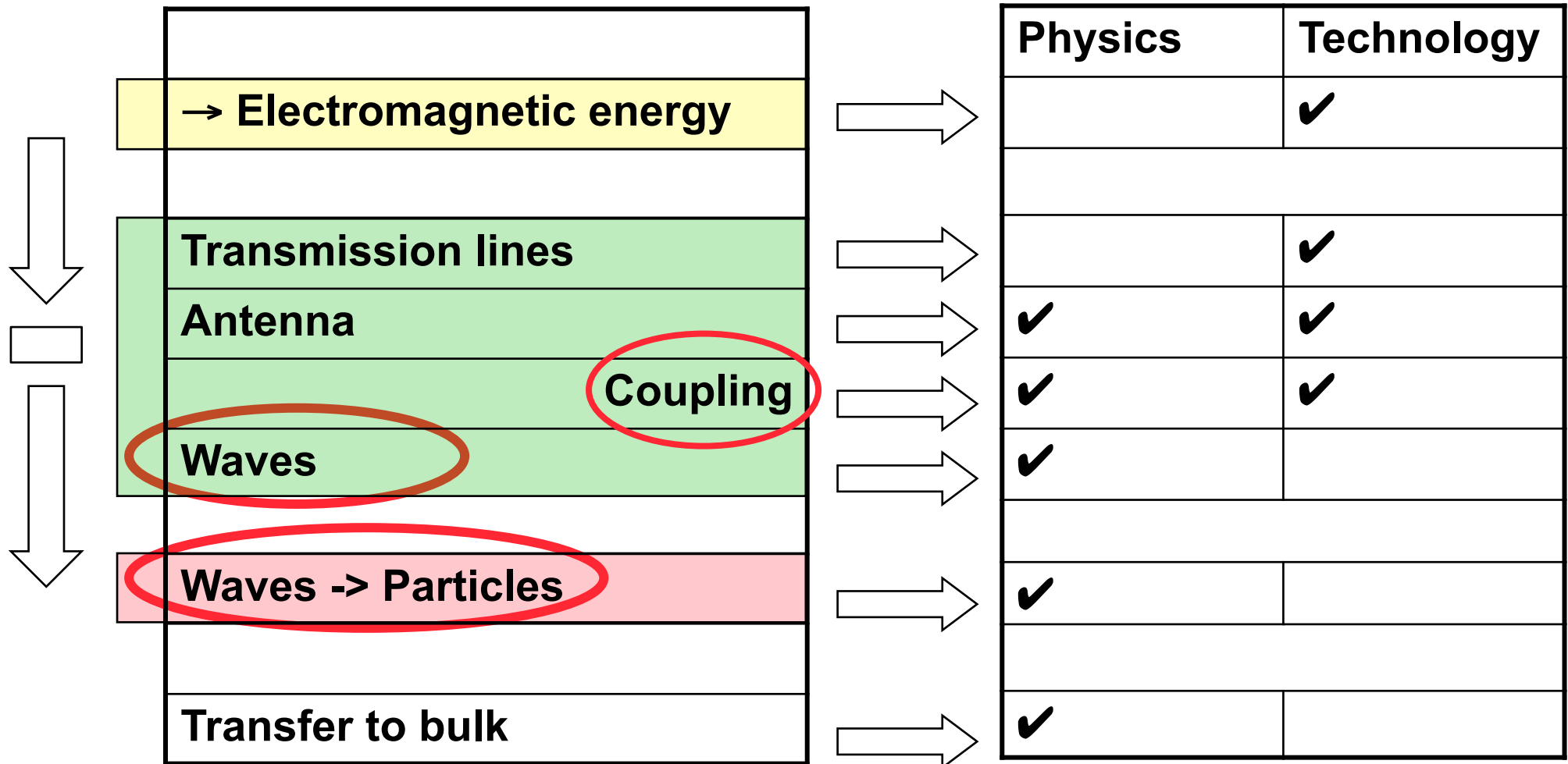
Wave heating

$$\Omega_c = \frac{Z e B}{m}$$



Wave heating: very tight combination of physics and technology

Wave propagation and **absorption** sets the frequency range that can be used.



Wave Equation

Maxwell's Equations

$$\begin{aligned}\nabla \times \quad \nabla \times \underline{E} &= -\frac{\partial \underline{B}}{\partial t} \\ \nabla \times \underline{B} &= \mu_0 \epsilon_0 \frac{\partial \underline{E}}{\partial t} + \mu_0 \underline{j} \\ \nabla \cdot \underline{E} &= \rho / \epsilon_0 \\ \nabla \cdot \underline{B} &= 0\end{aligned}$$

generalized Ohm's law

$$\underline{j} = \underline{j}(\underline{E}, \underline{B})$$

$$\underline{j}_{\omega, \underline{k}} = \underline{\sigma}(\omega, \underline{k}) \cdot \underline{E}_{\omega, \underline{k}}$$


$\underline{\sigma}$: conductivity tensor

Dispersion relation



- set of homogenous, linear equations for E_x , E_y , and E_z ,
- has non trivial (different from 0) solutions
provided the determinant vanishes
- $\det = 0$ is known as the **dispersion relation**
- **Existence of waves**
that transport energy from edge to inside the plasma

Dispersion relation, cold plasma case



$$\det[\underline{N} \times (\underline{N} \times \underline{1}) + \underline{K}(\omega, \underline{N})] = 0$$

$$A \cdot N^4 + B \cdot N^2 + C = 0$$

with

$$A = S \cdot \sin^2 \Theta + P \cdot \cos^2 \Theta$$

$$B = R \cdot L \cdot \sin^2 \Theta + P \cdot S \cdot (1 + \cos^2 \Theta)$$

$$C = P \cdot R \cdot L$$

$$N = \frac{c}{v_{ph}} = \frac{c \cdot k}{\omega}$$

$$S = \frac{1}{2}(R+L) \quad ; \quad D = \frac{1}{2}(R-L)$$

$$R = 1 - \frac{(\omega_{pe}/\omega)^2}{1 - \omega_{ce}/\omega} - \sum_i \frac{(\omega_{pi}/\omega)^2}{1 + \omega_{ci}/\omega}$$

$$L = 1 - \frac{(\omega_{pe}/\omega)^2}{1 + \omega_{ce}/\omega} - \sum_i \frac{(\omega_{pi}/\omega)^2}{1 - \omega_{ci}/\omega}$$

$$P = 1 - \left(\frac{\omega_{pe}}{\omega}\right)^2 - \sum_i \left(\frac{\omega_{pi}}{\omega}\right)^2$$

2 solutions for N^2

form of solution depends on S, P, R, L, Θ

Θ angle between \underline{k} and \underline{B}

$$tg^2 \Theta = - \frac{(N^2 - R) \cdot (N^2 - L) \cdot P}{(S \cdot N^2 - R \cdot L) \cdot (N^2 - P)}$$

Characteristic frequencies

Plasmafrequencies

$$\omega_{pe}^2 = \frac{e^2 n_e}{\epsilon_0 m_e}$$

$$\omega_{pi}^2 = \frac{(Z_i e)^2 n_i}{\epsilon_0 m_i}$$

$$R = 1 - \frac{(\omega_{pe}/\omega)^2}{1 - \omega_{ce}/\omega} - \sum_i \frac{(\omega_{pi}/\omega)^2}{1 + \omega_{ci}/\omega}$$

$$L = 1 - \frac{(\omega_{pe}/\omega)^2}{1 + \omega_{ce}/\omega} - \sum_i \frac{(\omega_{pi}/\omega)^2}{1 - \omega_{ci}/\omega}$$

$$P = 1 - \left(\frac{\omega_{pe}}{\omega}\right)^2 - \sum_i \left(\frac{\omega_{pi}}{\omega}\right)^2$$

Cyclotron frequencies

$$\omega_{ce} = \frac{eB}{m_e}$$

$$\omega_{ci} = \frac{Z_i eB}{m_i}$$

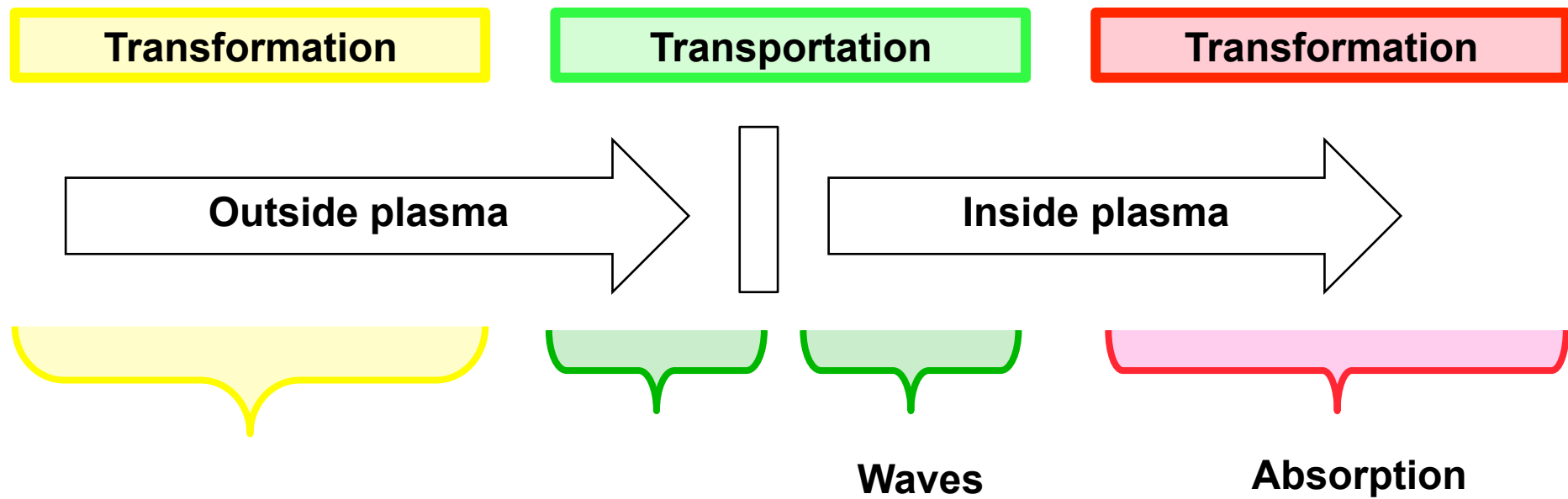
Upper Hybrid frequency

$$\omega_{uh}^2 = \omega_{pe}^2 + \omega_{ce}^2$$

Lower Hybrid frequency

$$\omega_{lh}^2 = \left[\frac{1}{\omega_{pi}^2 + \omega_{ci}^2} + \frac{1}{\omega_{ci}\omega_{ce}} \right]^{-1}$$

Requirements

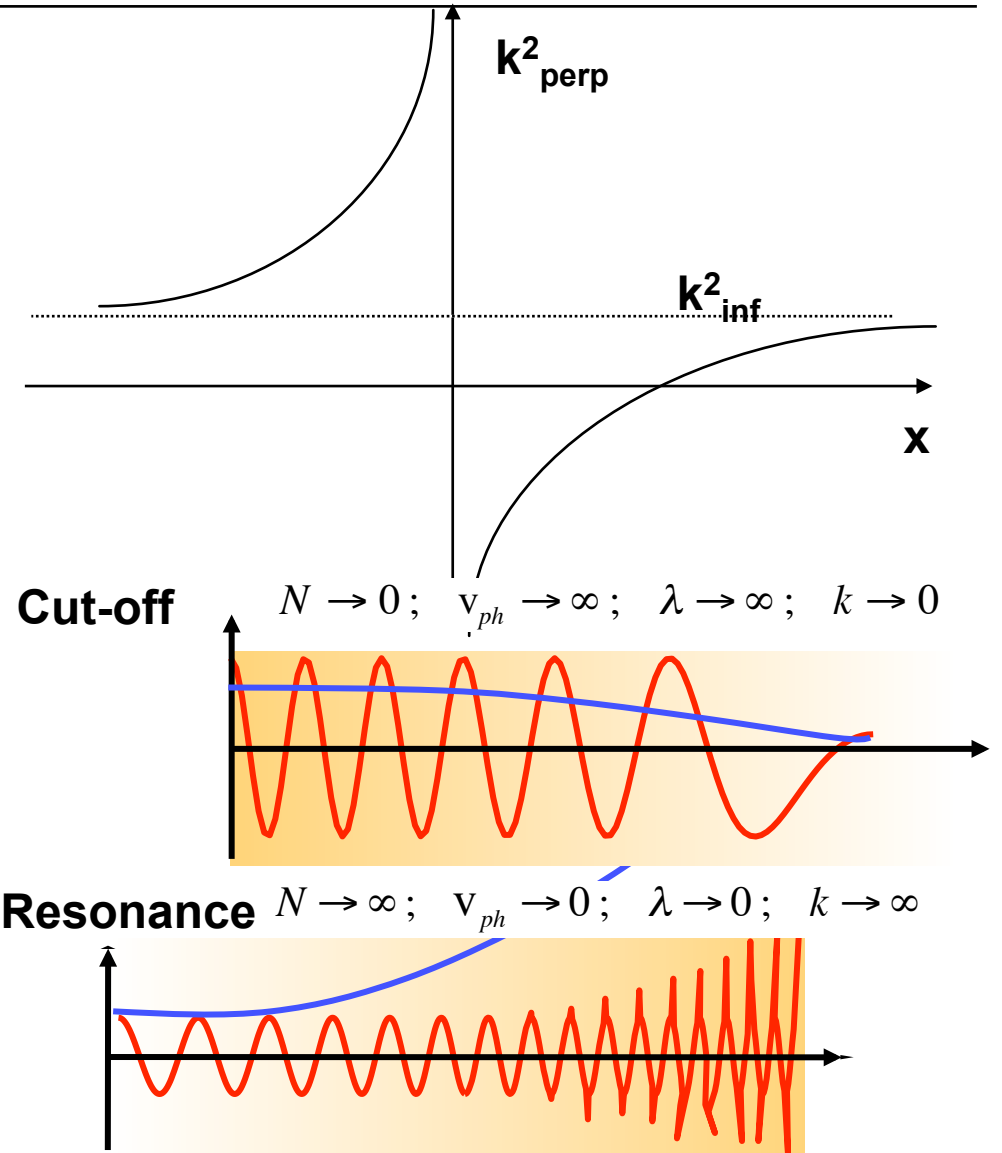


- **2 solutions for $(k/k_0)^2$, function of Θ**

- if > 0 -> propagating
- if < 0 -> non-propagating

- **$(k/k_0)^2$ can change sign**

- by going through 0 -> cut-off
 - reflection
 - evanescent wave
- by going through infinity -> resonance
 - absorption
 - reflection and transmission



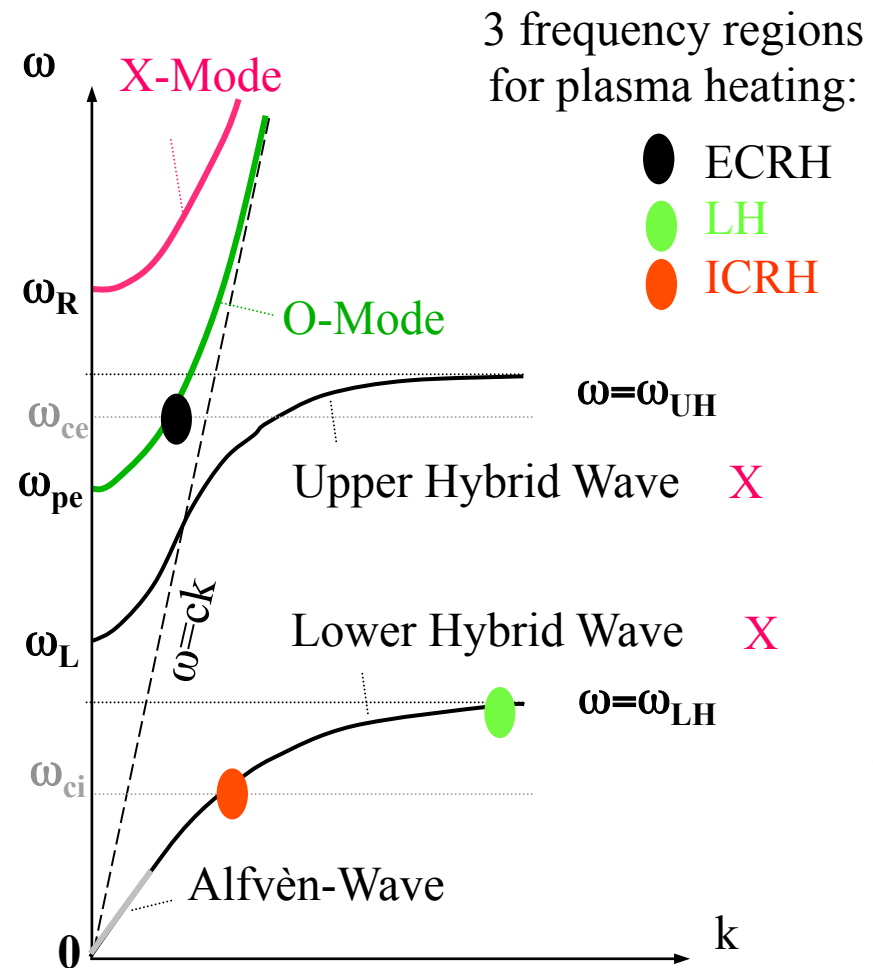
Wave propagation and absorption

$$\operatorname{tg}^2 \Theta = - \frac{(N^2 - R) \cdot (N^2 - L) \cdot P}{(S \cdot N^2 - R \cdot L) \cdot (N^2 - P)}$$

$$k \perp B \rightarrow \Theta = \pi/2$$

$$N^2 = P \rightarrow \text{O - mode}$$

$$N^2 = \frac{RL}{S} \rightarrow \text{X - mode}$$



Wave propagation and absorption

- **ECRH**

- electron cyclotron resonance heating

- **LH**

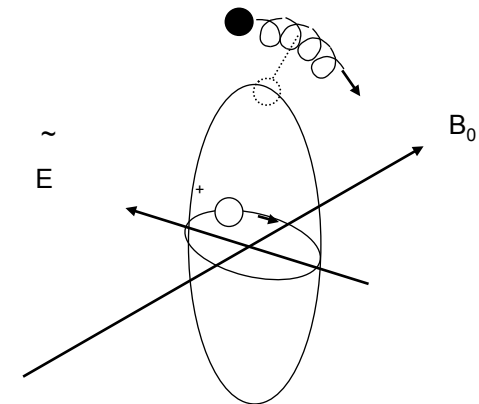
- lower hybrid frequency $\omega_{ci} \ll \omega \ll \omega_{ce}$

ion unmagnetized, oscillate with E_1

electrons oscillate with $E_1 \times B_0$ drift

- **ICRF**

- ion cyclotron range of frequencies



Transport from outside plasma to inside: wave propagation

(wave cut-off and resonance)

Transfer of energy from wave to particles: particle resonance condition

(wave-particle interaction)

Absorption: Collisionless Damping

Energy transfer only if

$$\omega - n\omega_c = k_{\parallel}v_{\parallel}$$

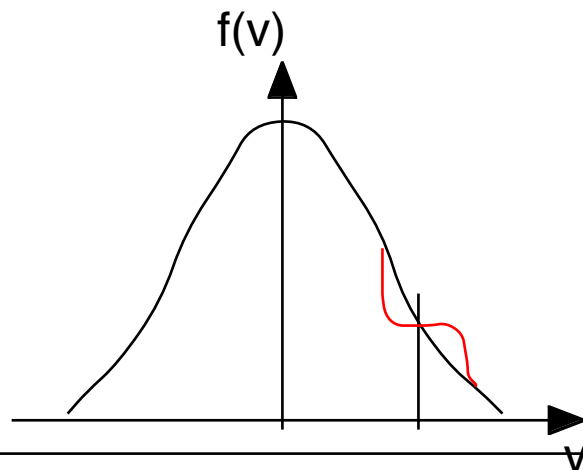
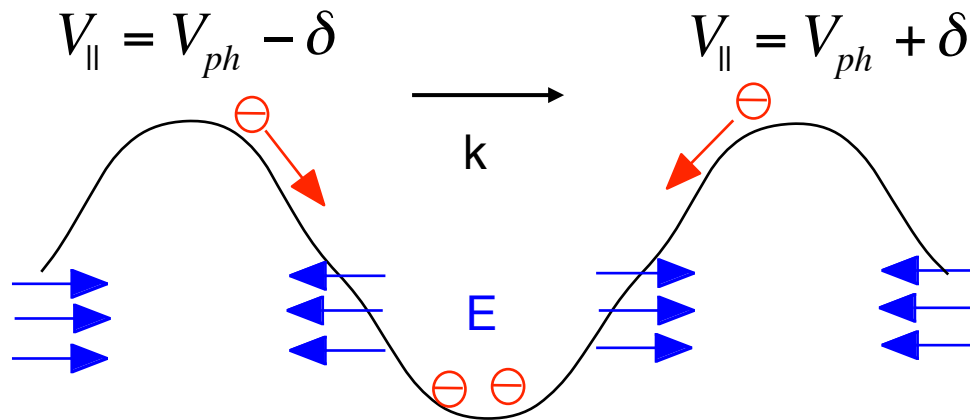
$$n = 0$$

Resonance condition:

$$\omega - k_{\parallel}v_{\parallel} = 0$$

Condition for damping

$$\frac{\partial f(v)}{\partial v} < 0$$



The deformation of the distribution function increases the energy of the electron system.

Landau damping: Increase of parallel momentum

Cyclotron Damping (Doppler shifted)

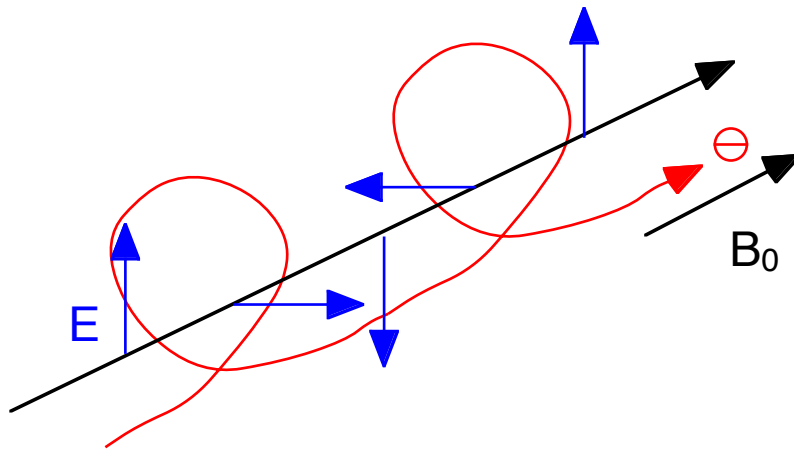
Energy transfer only if

$$\omega - n\omega_c = k_{\parallel}v_{\parallel}$$

$$n = 1$$

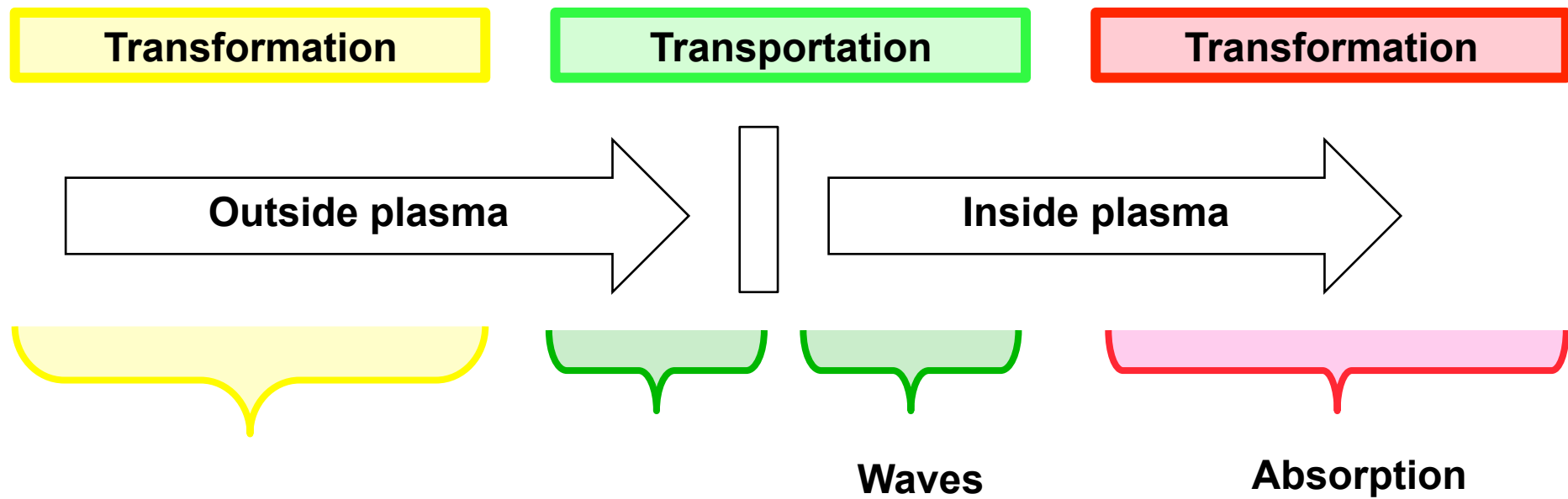
Resonance condition:

$$\omega - k_{\parallel}v_{\parallel} = \omega_c$$

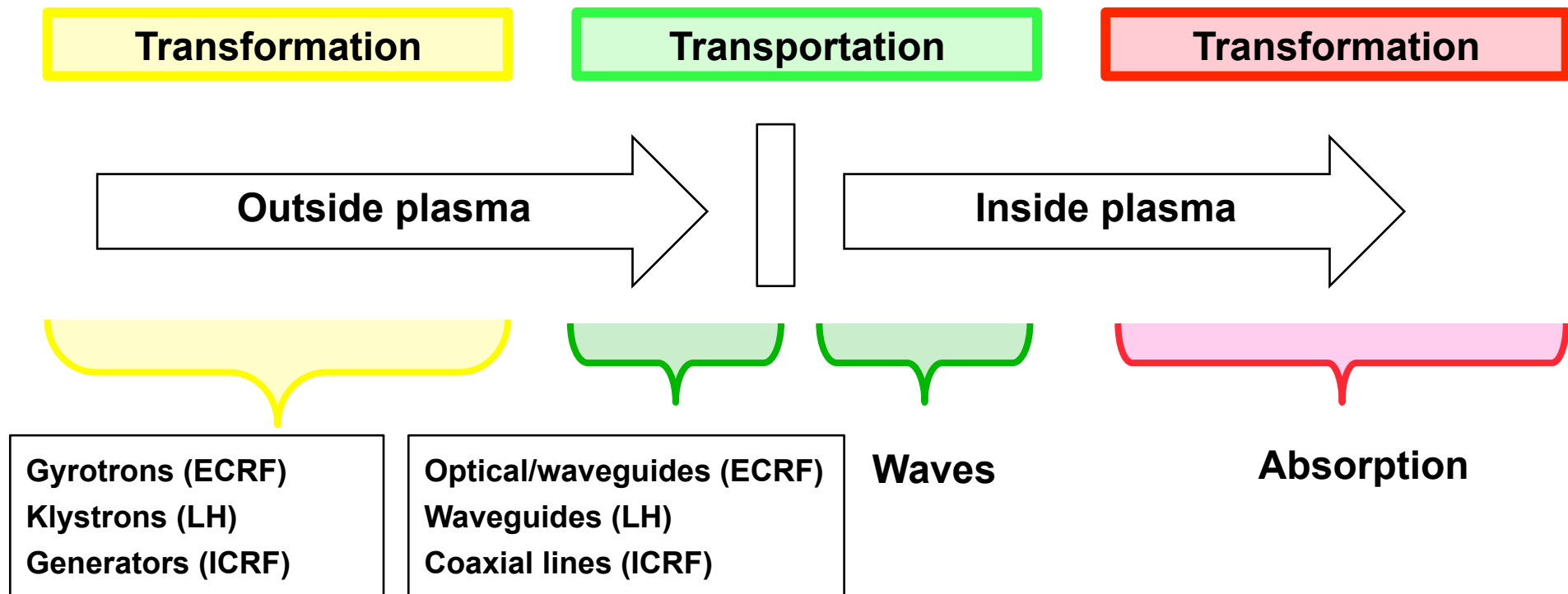


Cyclotron Damping: increase of perpendicular momentum

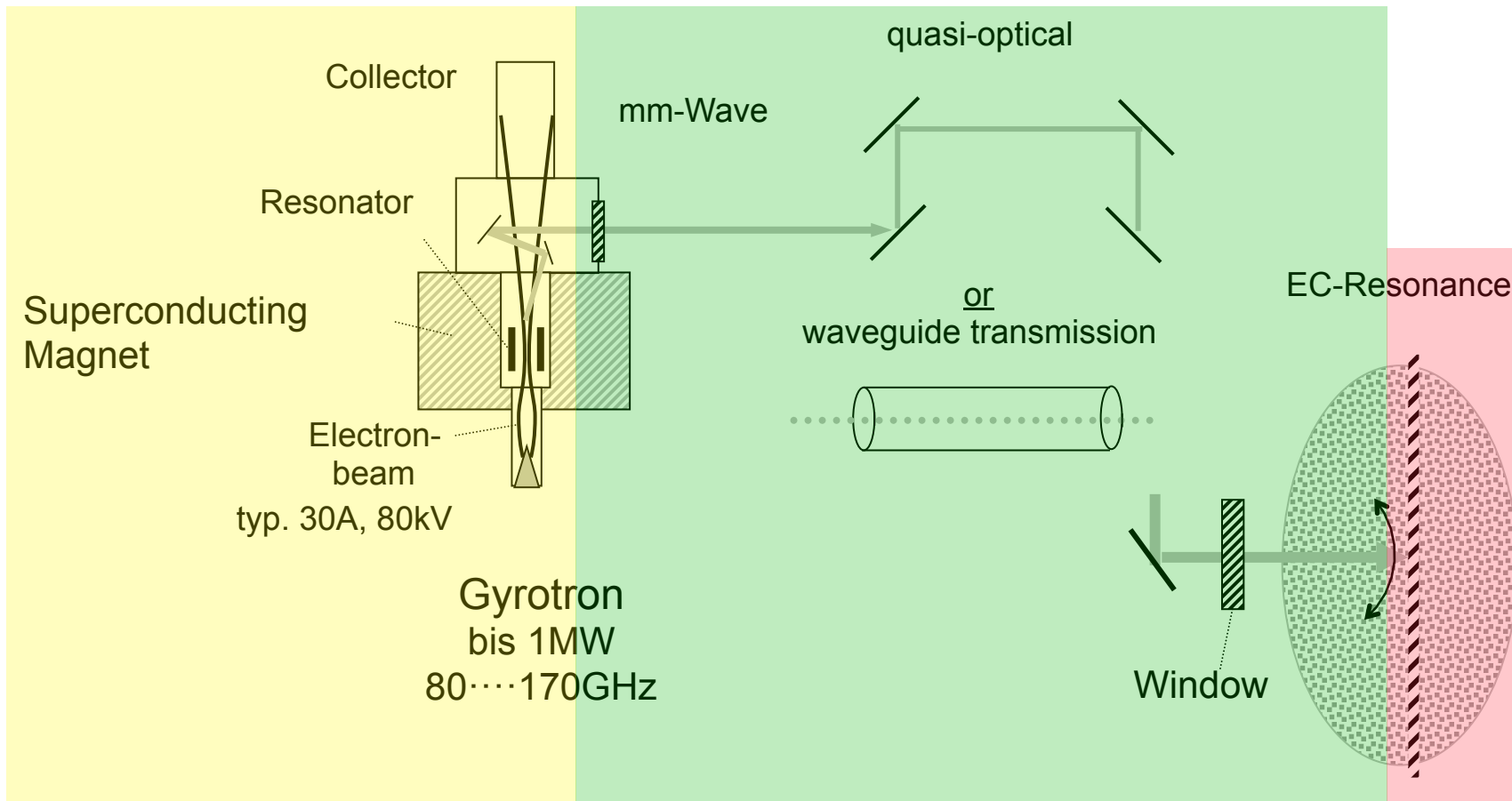
Requirements



Requirements



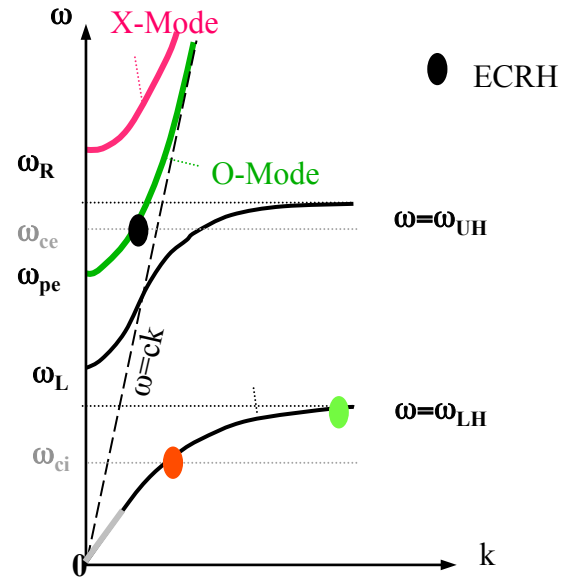
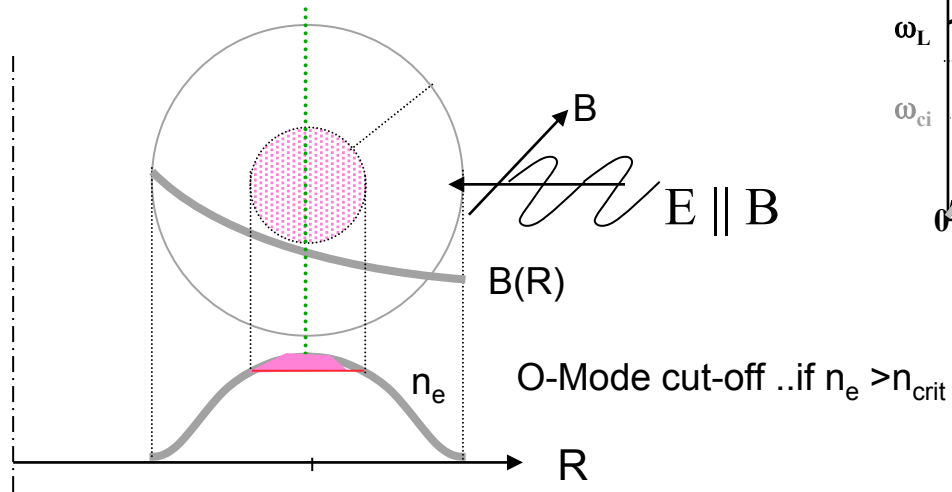
ECRH System



ECR

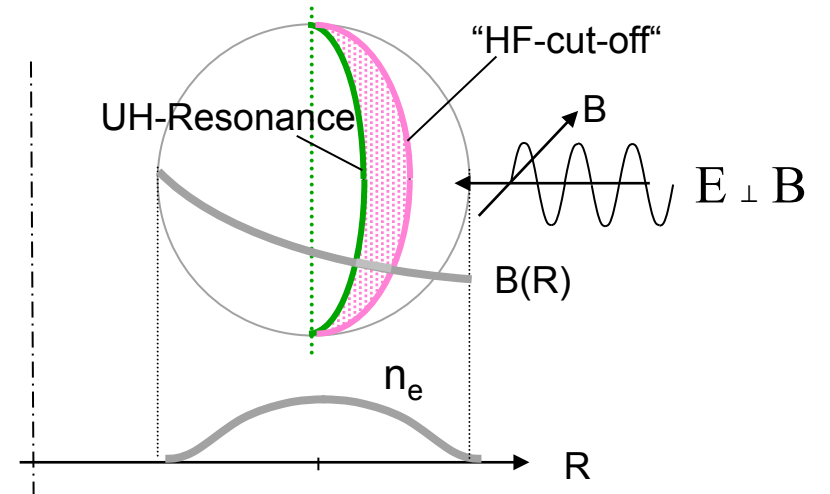
O-Mode

EC-“Resonance“

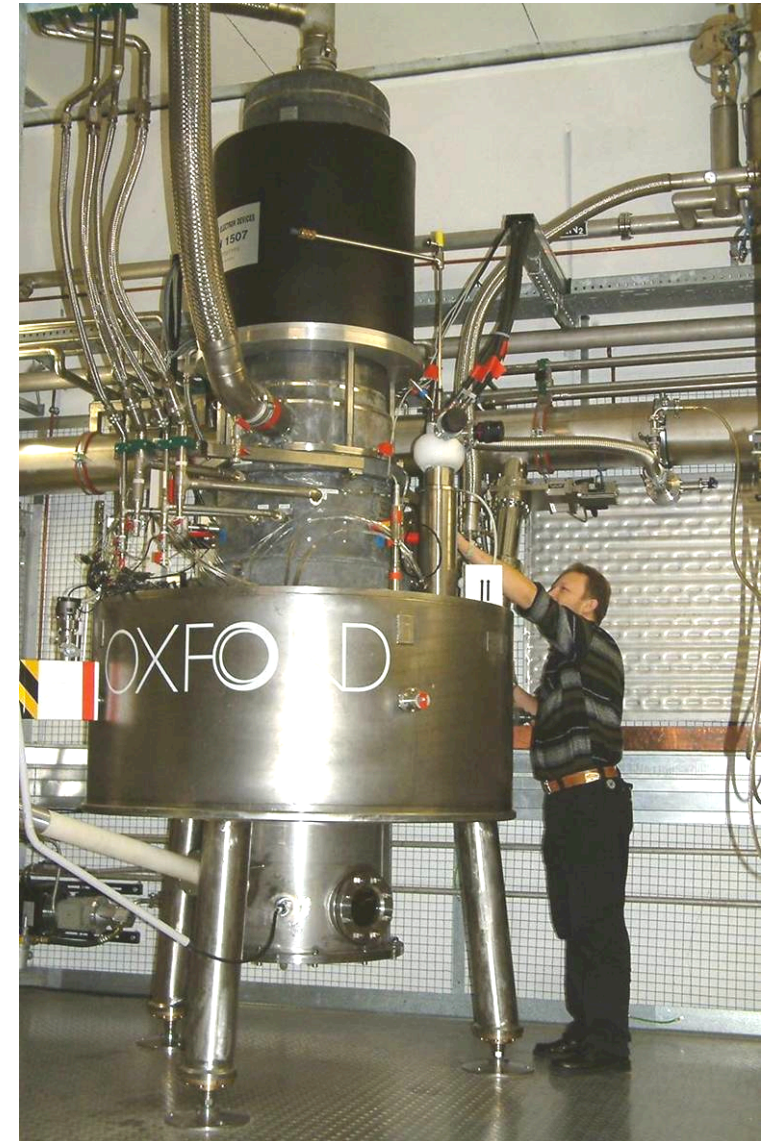
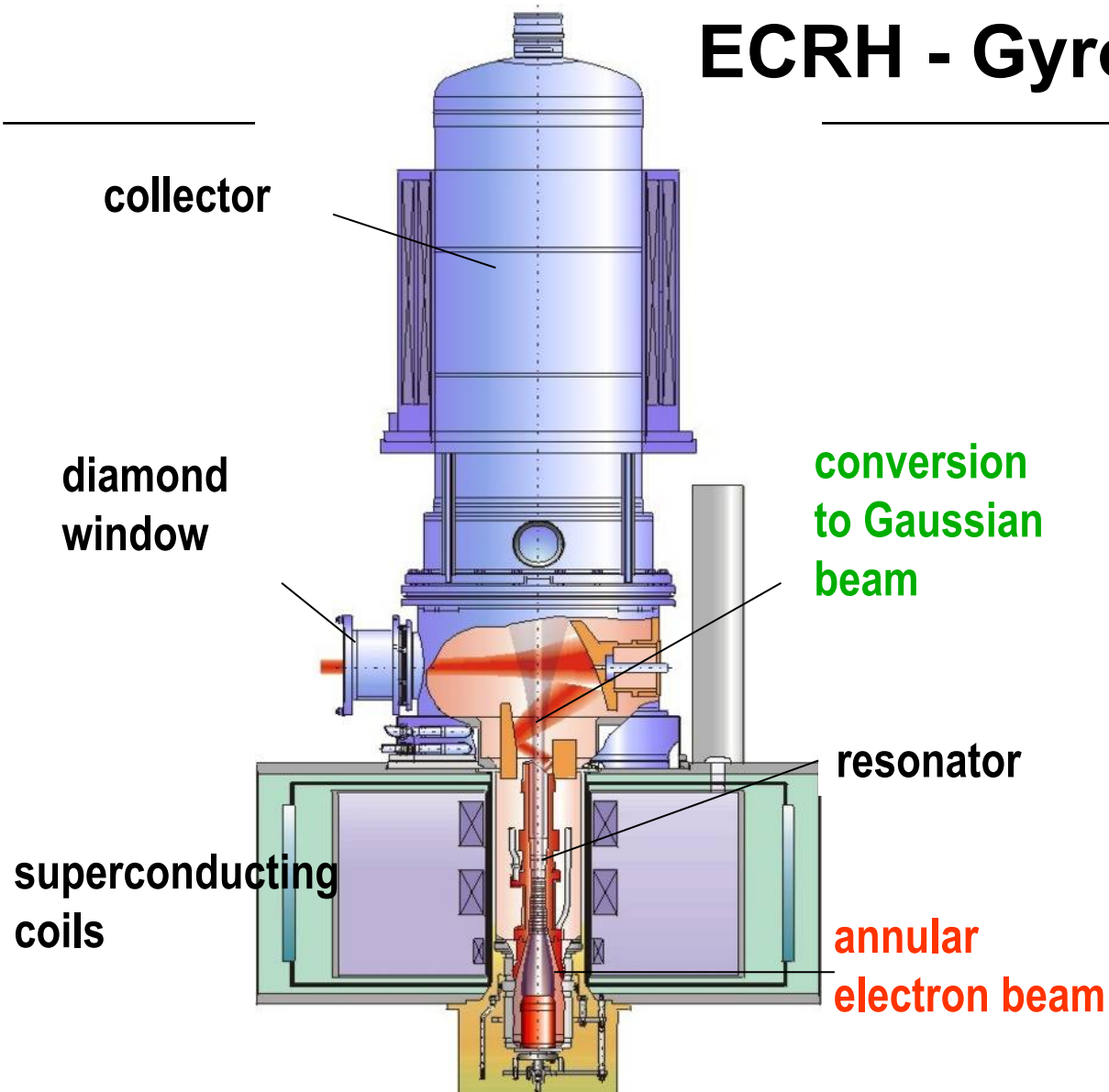


X₁-Mode

EC-“Resonance“



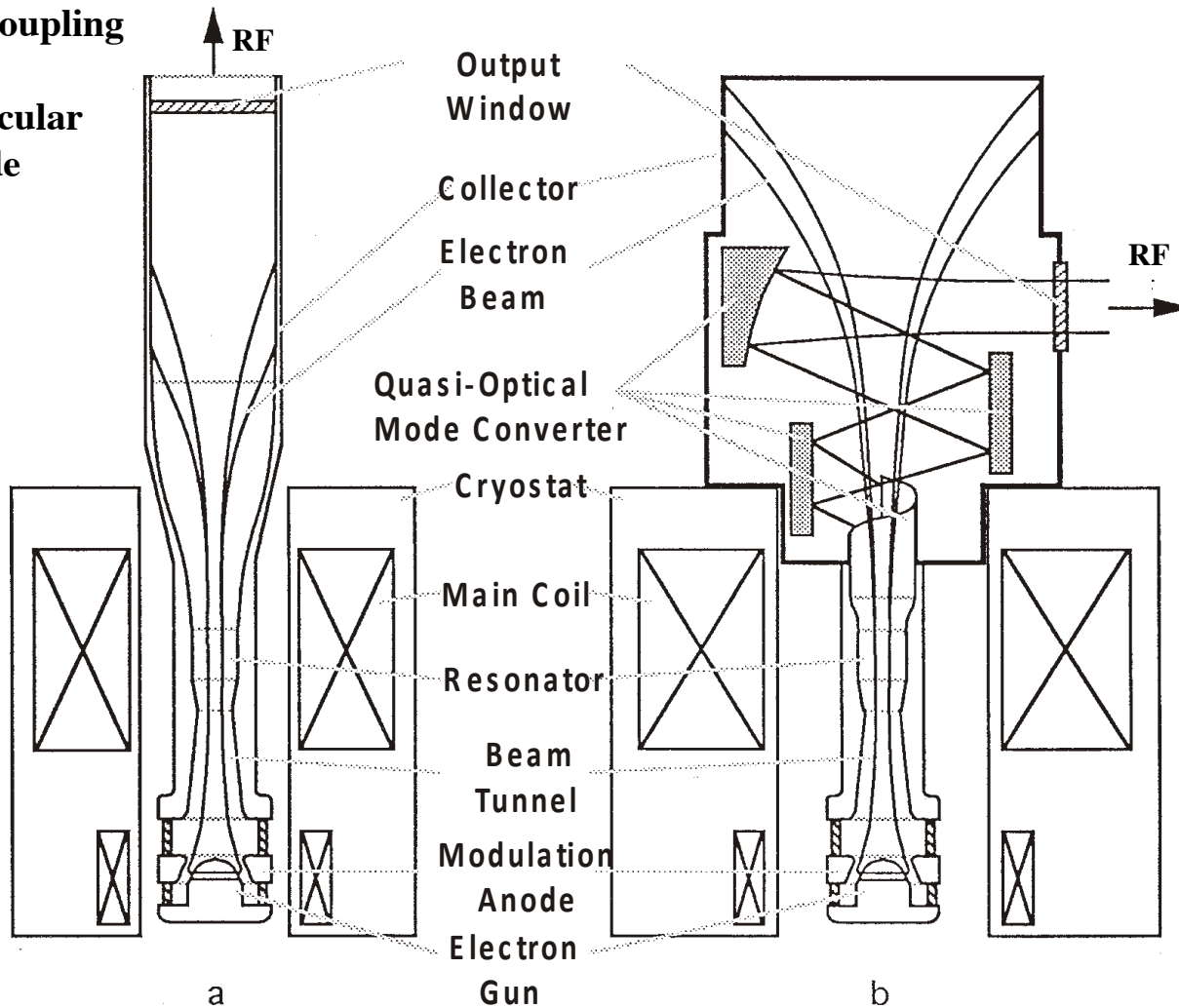
ECRH - Gyrotrons



Presently: development of 1 MW cw gyrotrons

Quasi-Optical Output Couplers for High-Power Gyrotrons (1975 Russia)

**Axial Output Coupling
through
Oversized Circular
Waveguide
e.g. TE_{03}**

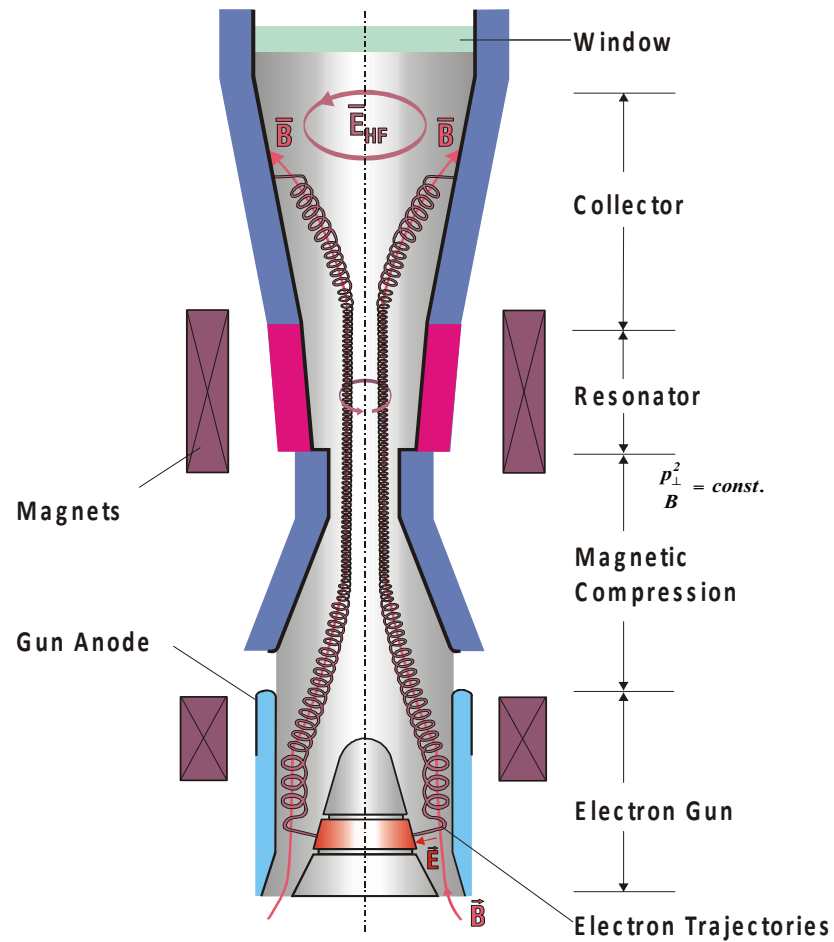


**Radial Output Coupling
through
Optical Elements
 TEM_{00} (Gaussian Beam)**

Advantages :

- **Isolator for Reflections**
- **Optimum Mode for Transmission**
- **Free Choice of Collector Design**

Further developments



Separate window and collector

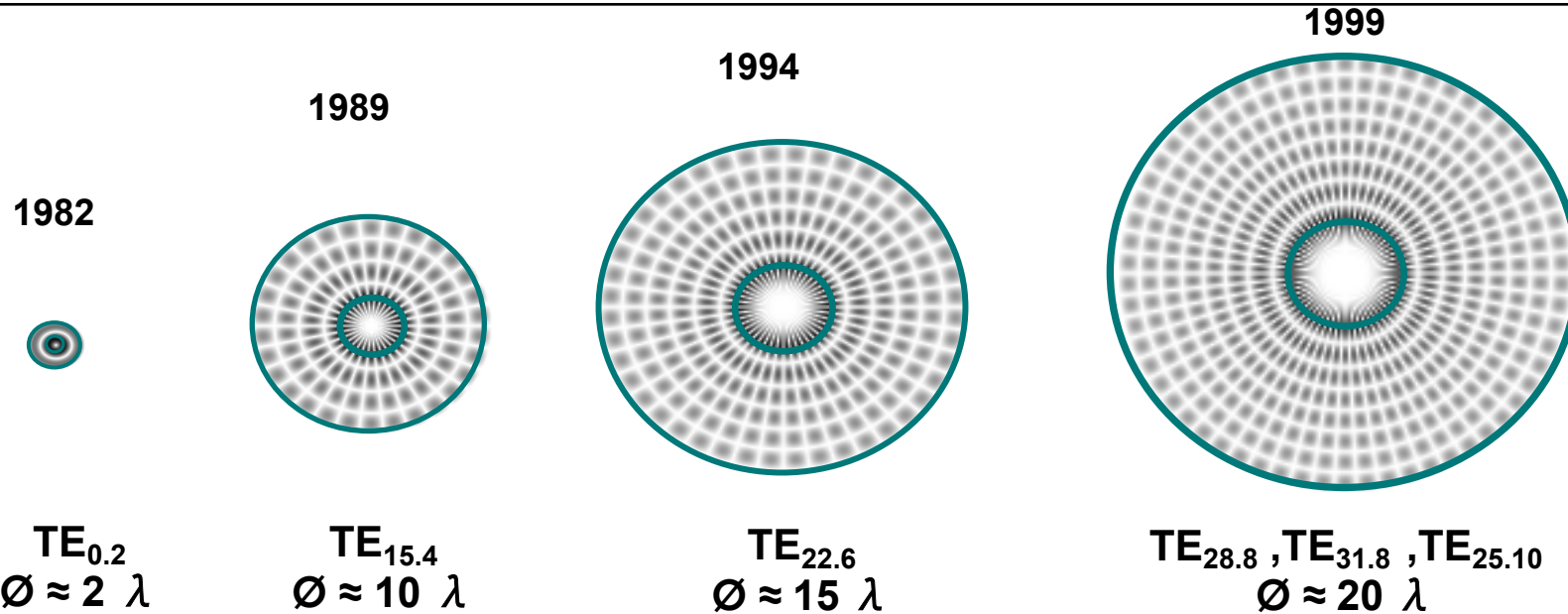
Diamond window

Biased collector

Multimode cavity

Coaxial cavity

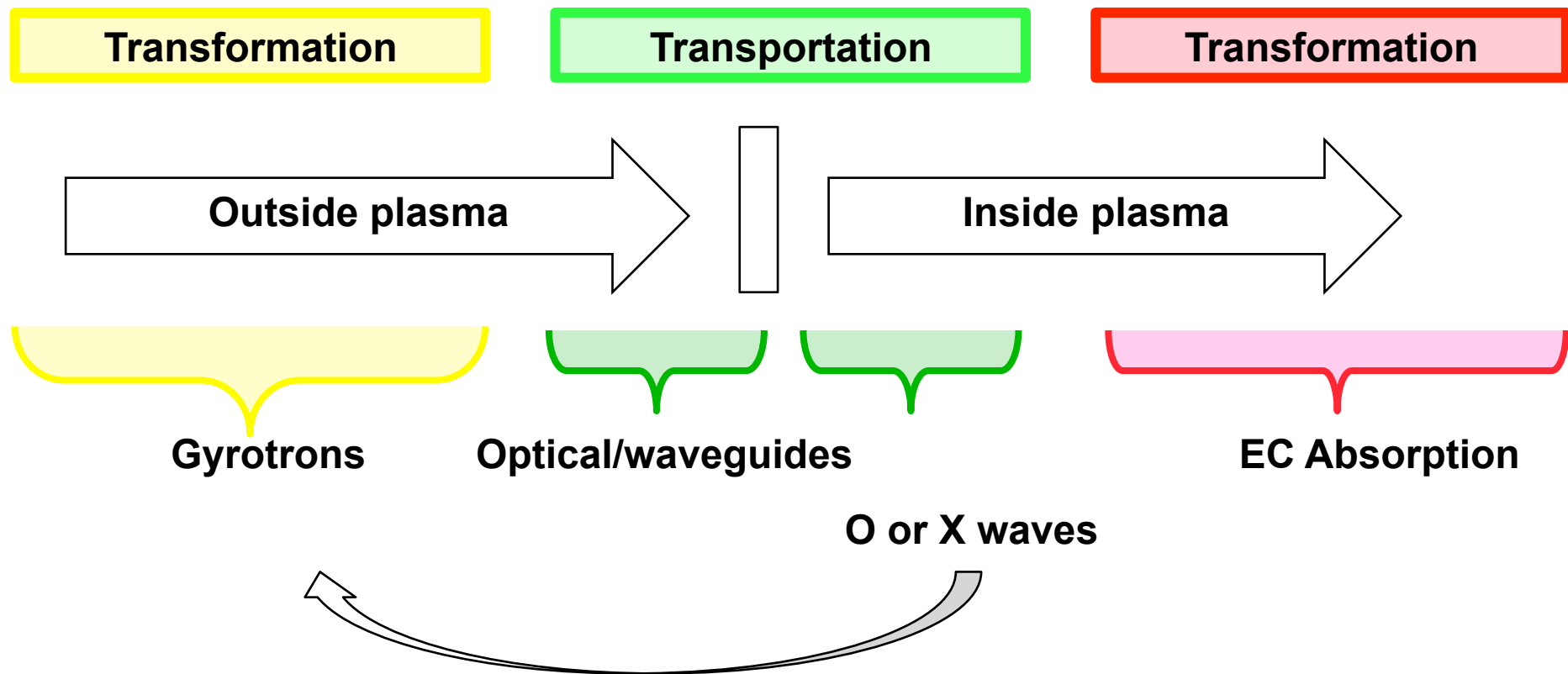
High-Order Volume-Mode Operation in Gyrotron



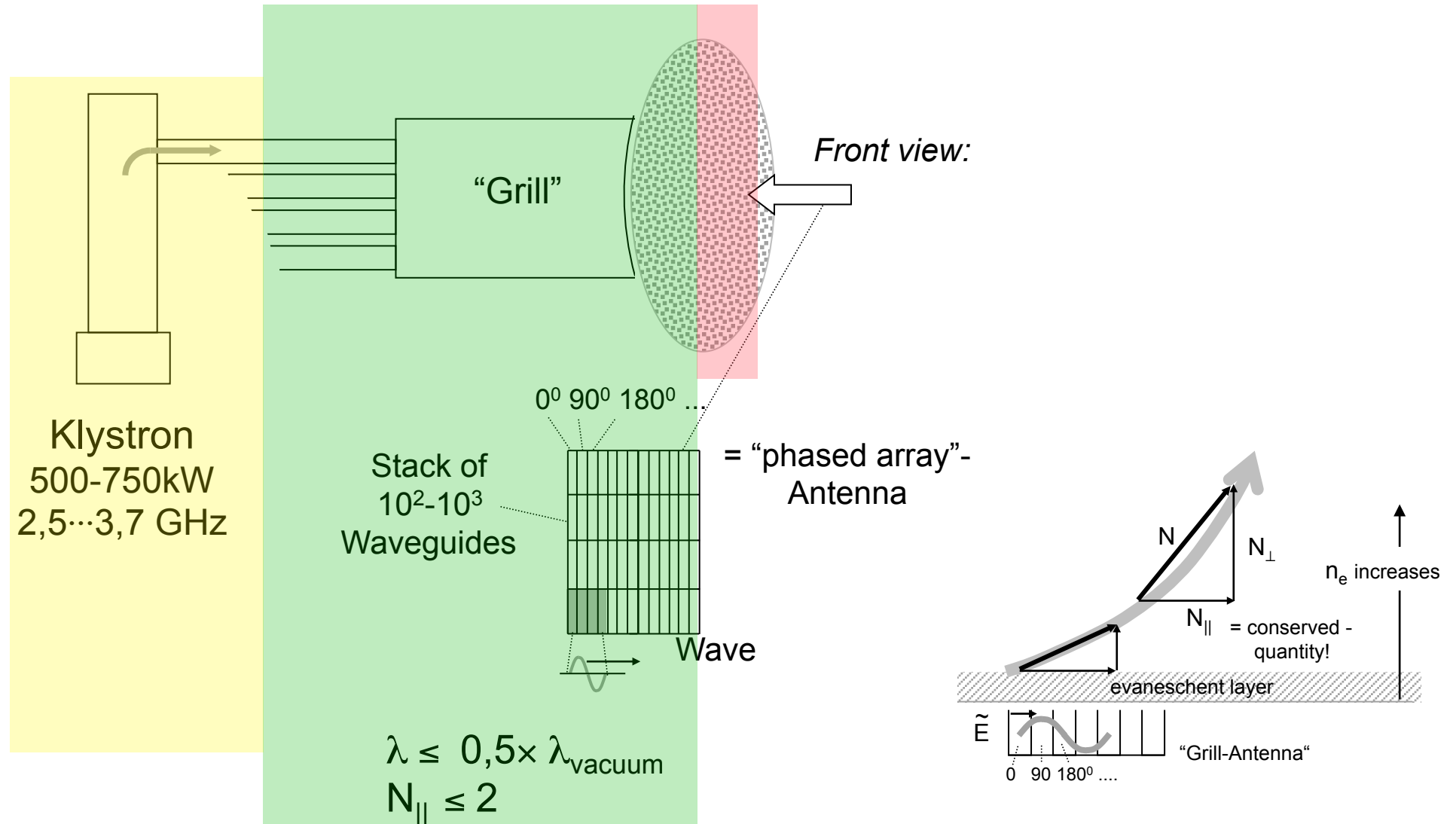
- electron beam on the first maximum (on the modal caustic)
⇒ reduced mode competition
- smooth diameter transitions
⇒ high mode purity (99%)
- dispersion strengthened copper (Al_2O_3)
⇒ improved thermo-mechanical features

$TE_{28.8}$: EU	140 GHz (W-7X)
$TE_{31.8}$: JA	170 GHz (ITER)
$TE_{25.10}$: RF	170 GHz (ITER)

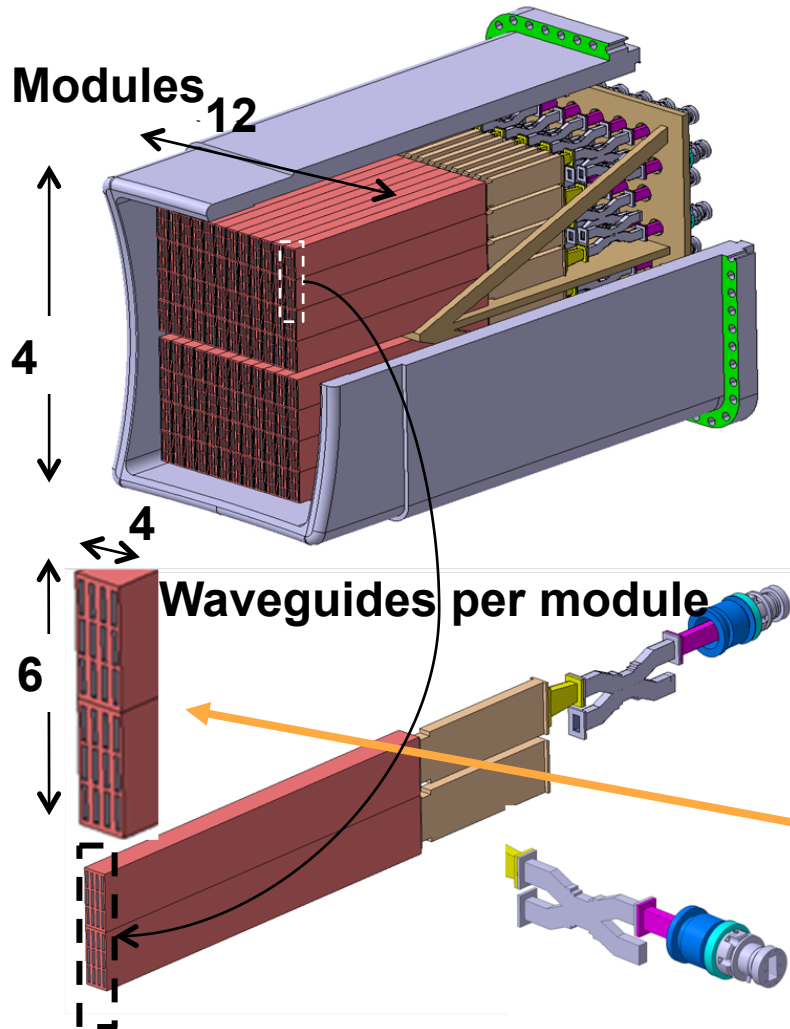
ECRH



Lower Hybrid system



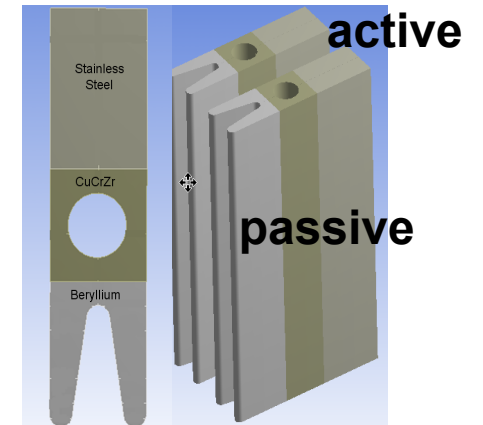
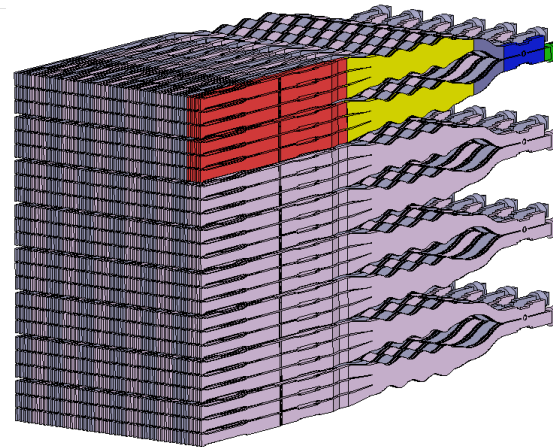
Passive Active Multi-junction Launcher Concept (PAM)



48 modules of

6 (poloidal direction) x 4 (toroidal direction) active WG

1152 active waveguides (WG)



One module:

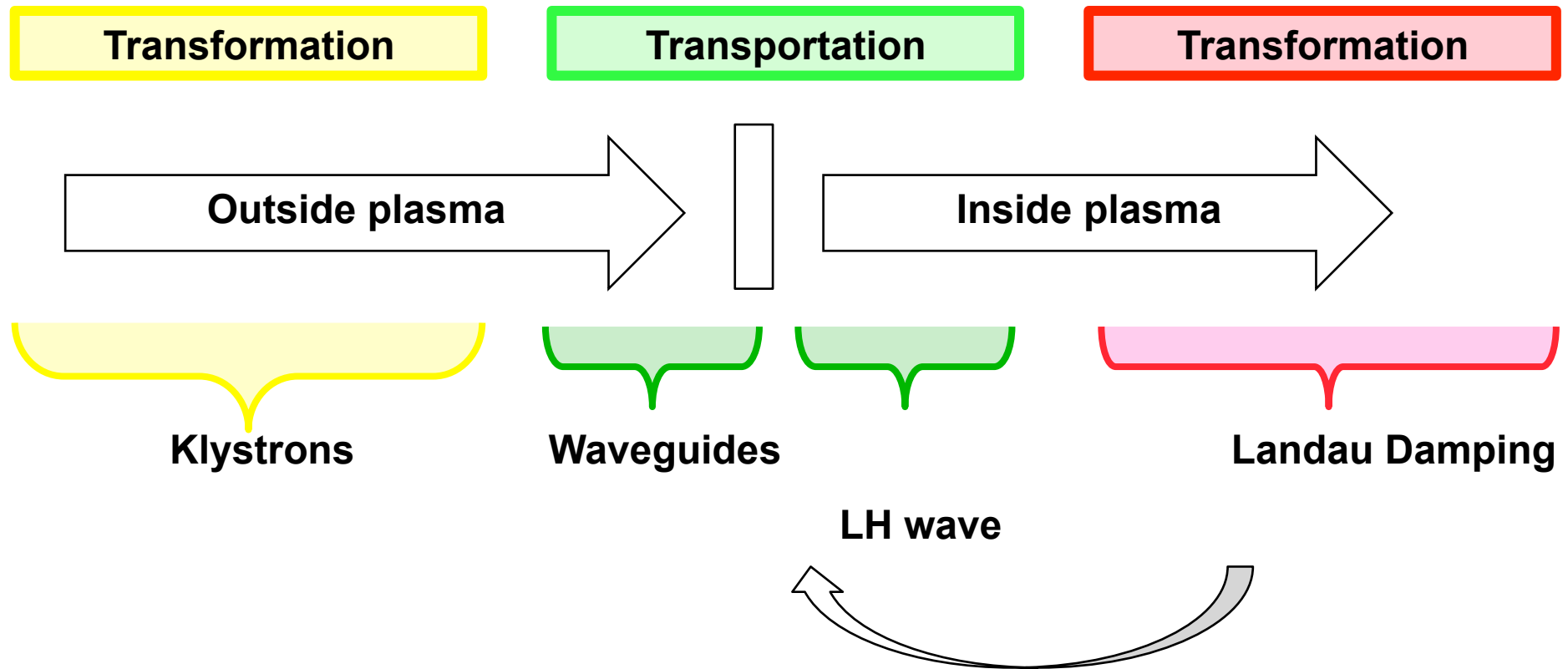
6 rows of multi-junction (6 x 4 active WGs)

2 mode converters,

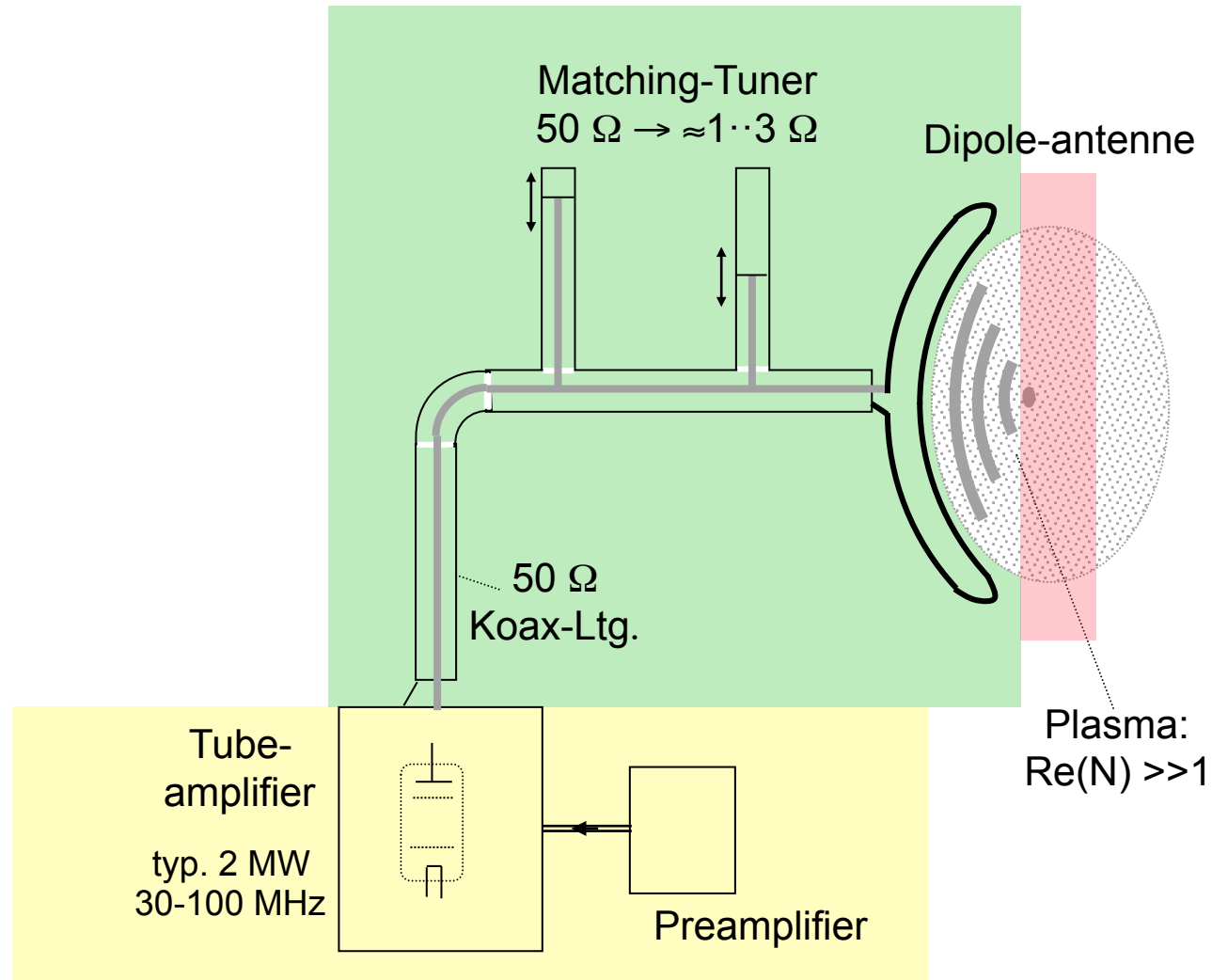
2 tapers, 1 splitter,

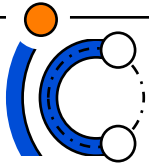
1 transmission line, 1 bellow, 1 window

LH



Ion cyclotron system





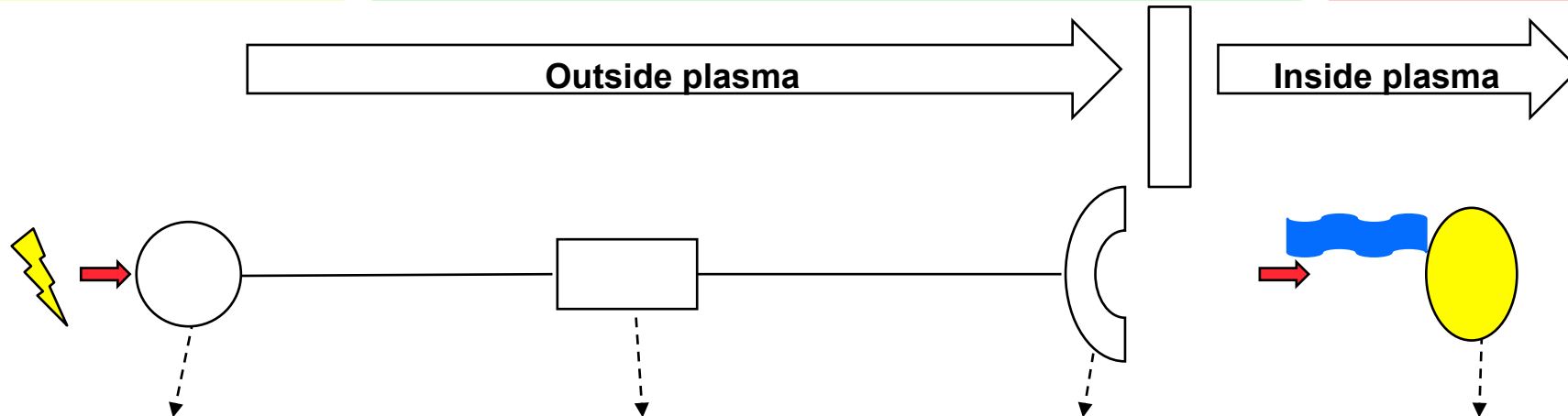
The ASDEX Upgrade ICRF system



Transformation

Transportation

Transformation



Generators



Lines and matching

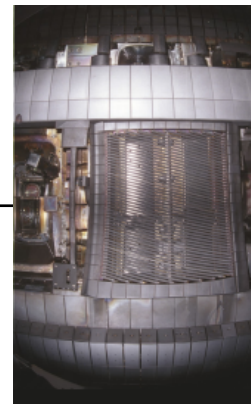
3 dB-couplers



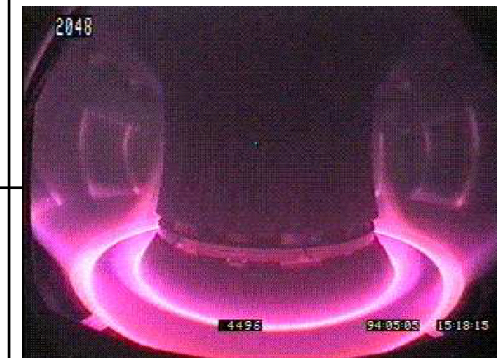
tuners



Antenna

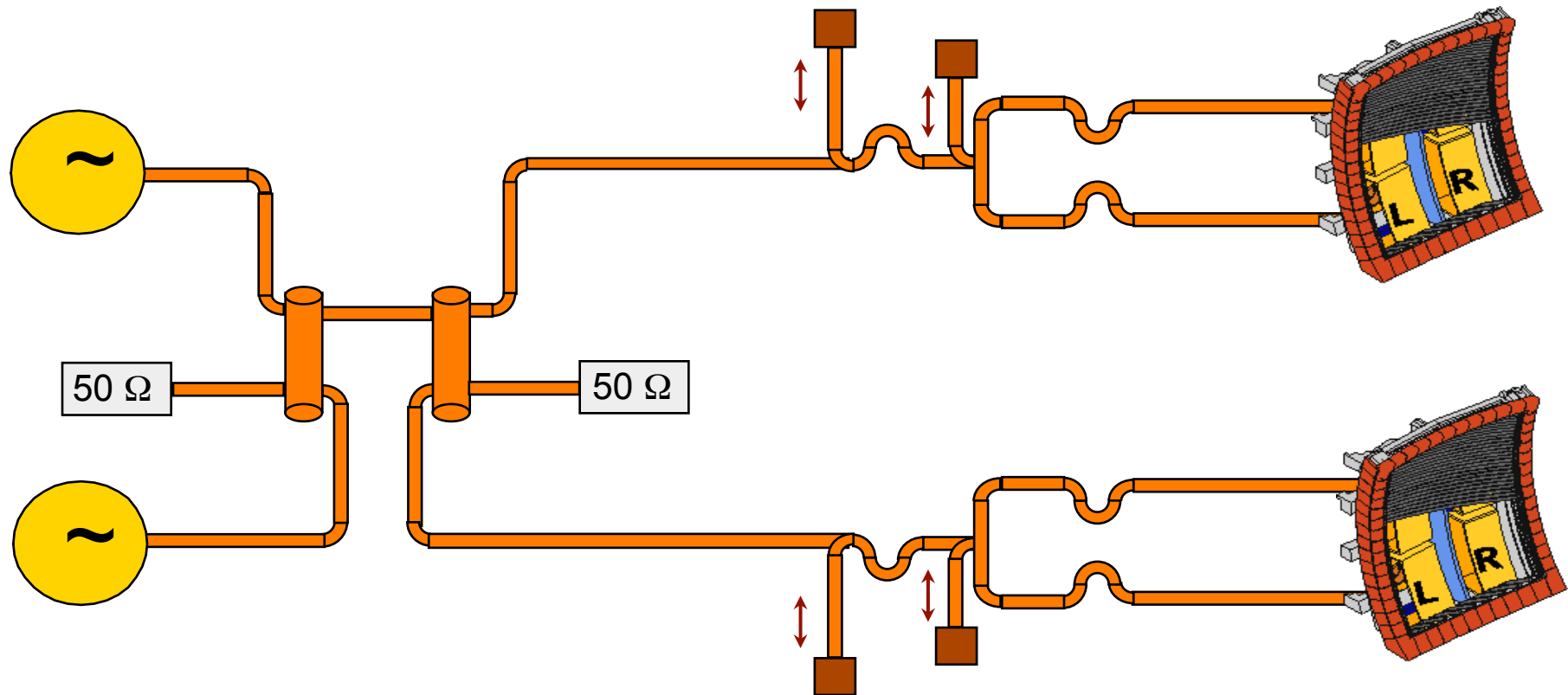


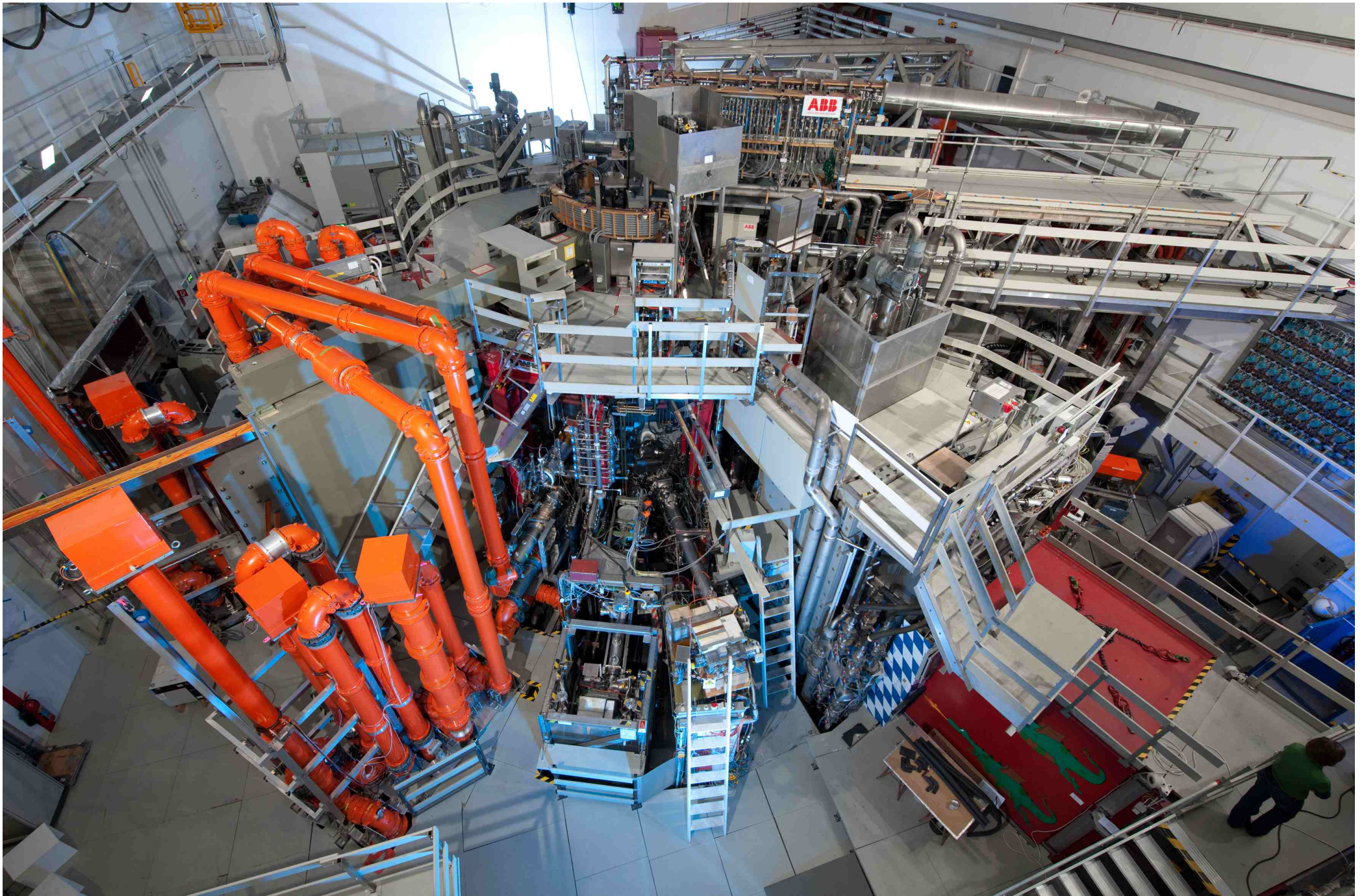
Plasma



Transmission lines

3 dB couplers and dummy loads





Waveguides would be too large

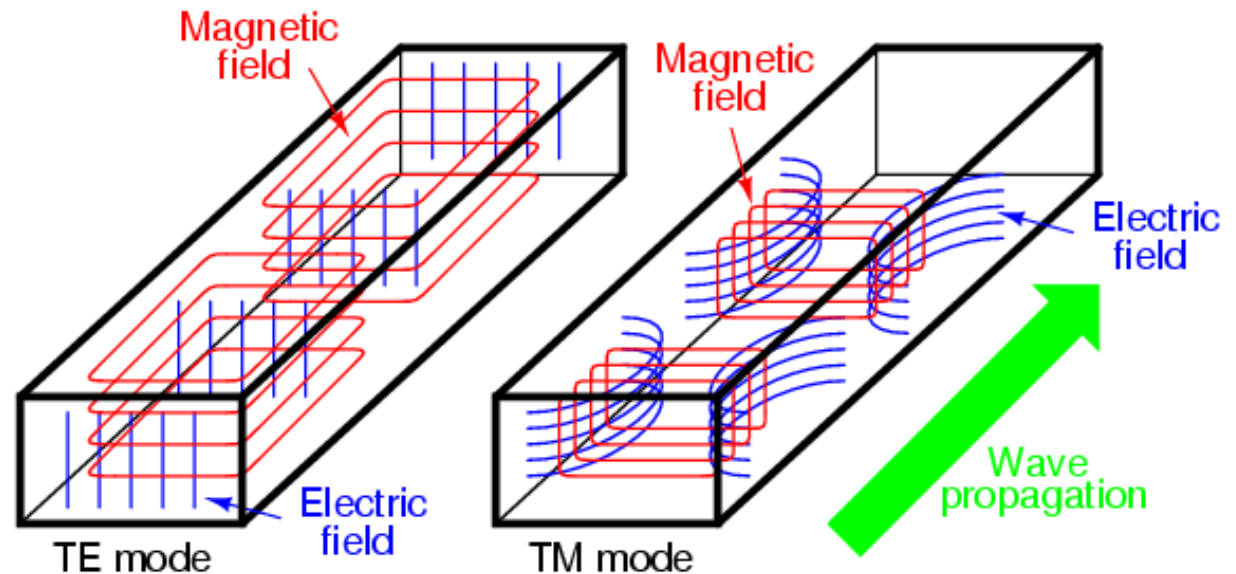
- Transfer to plasma, outside of the machine
 - free space propagation: space \gg wavelength = 10m at 30 MHz
 - waveguide propagation: lower frequency cut-off of waveguide: dimensions $>$ wavelength/2 = 5m at 30 MHz

TE01

$$\lambda_c = \frac{2}{\sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2}} = 2a$$

TM11

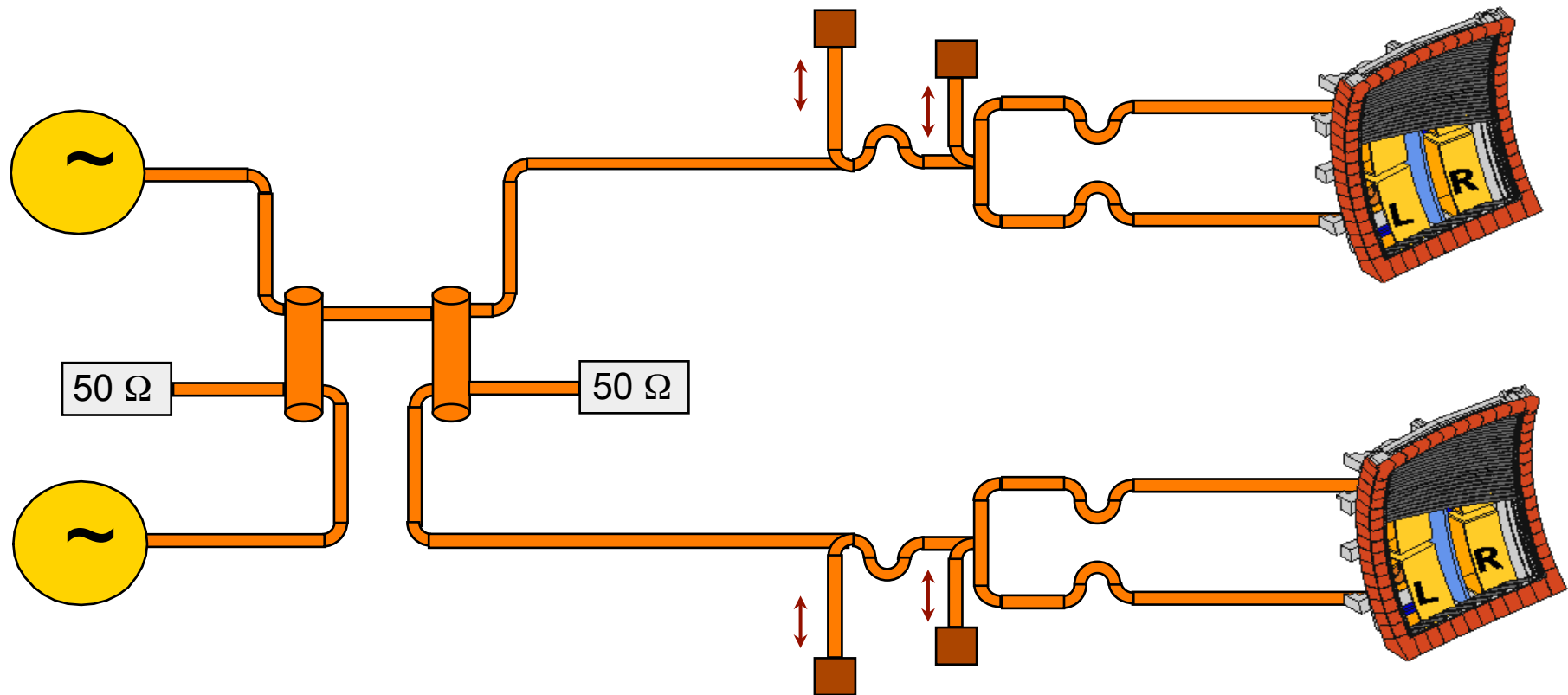
$$\lambda_c = \frac{2}{\sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2}} = a\sqrt{2}$$



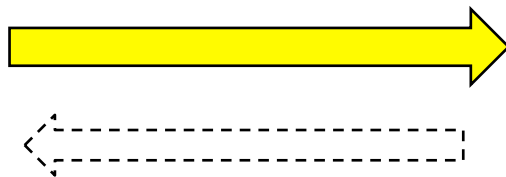
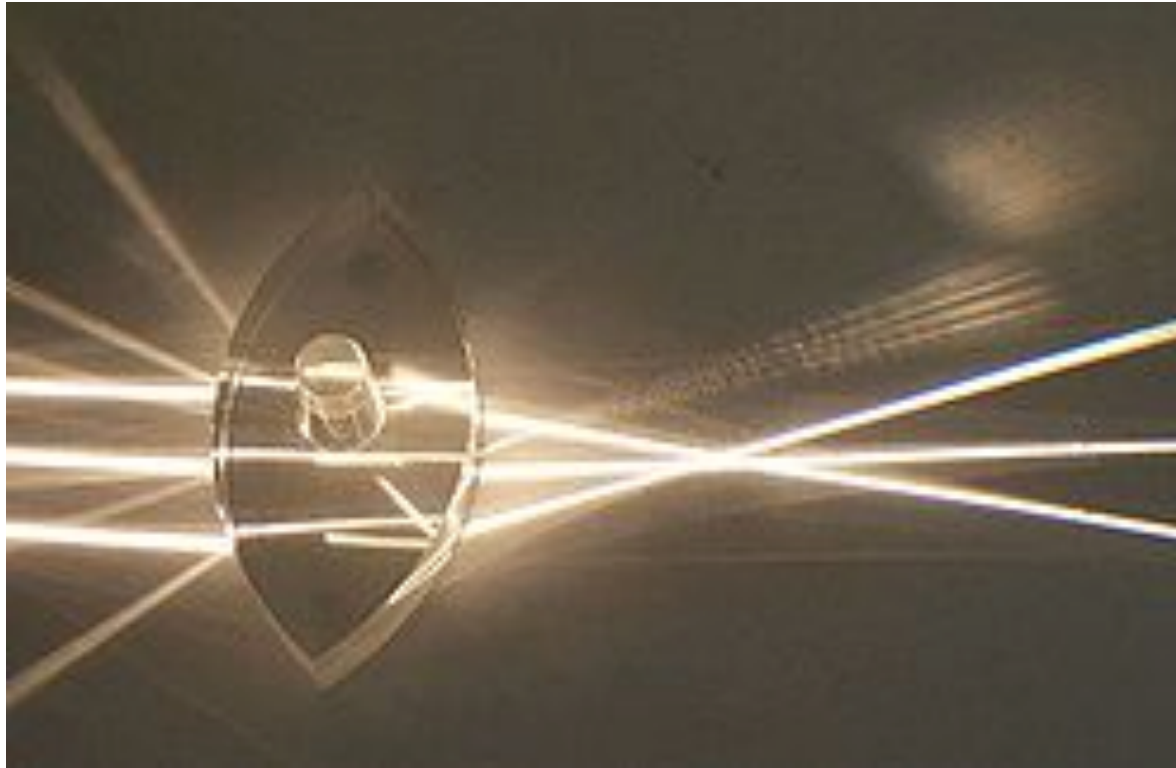
Magnetic flux lines appear as continuous loops
Electric flux lines appear with beginning and end points

Transmission lines

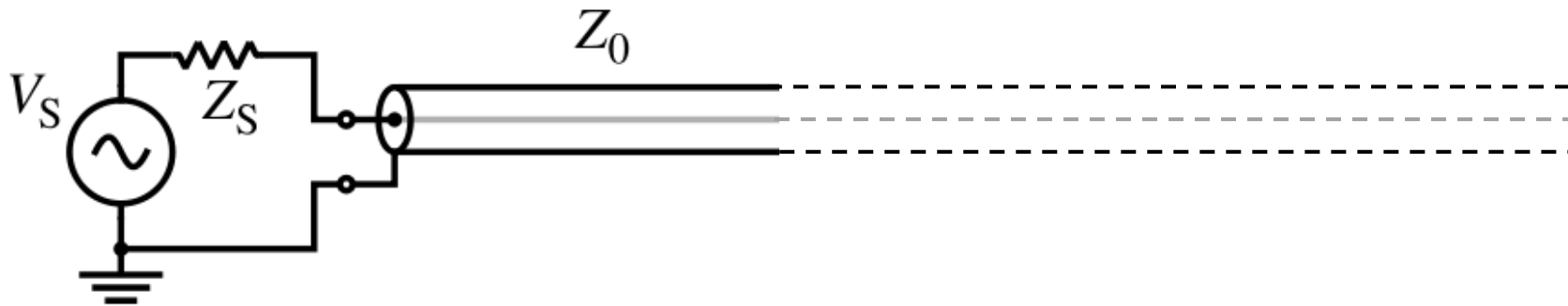
3 dB couplers and dummy loads



Backward waves are **reflected** waves generated at **changes**
in the properties of propagating medium

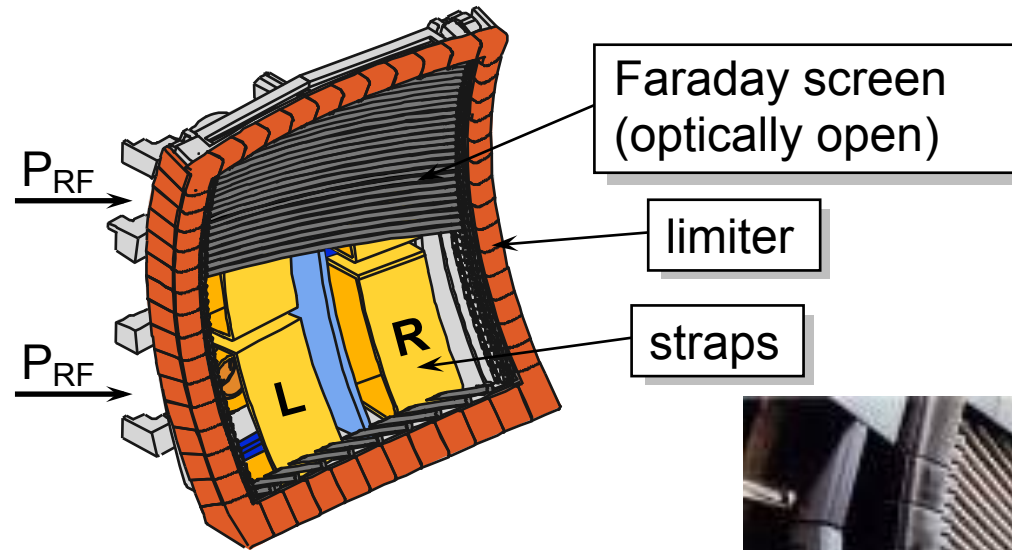


What are the properties of a transmission line?



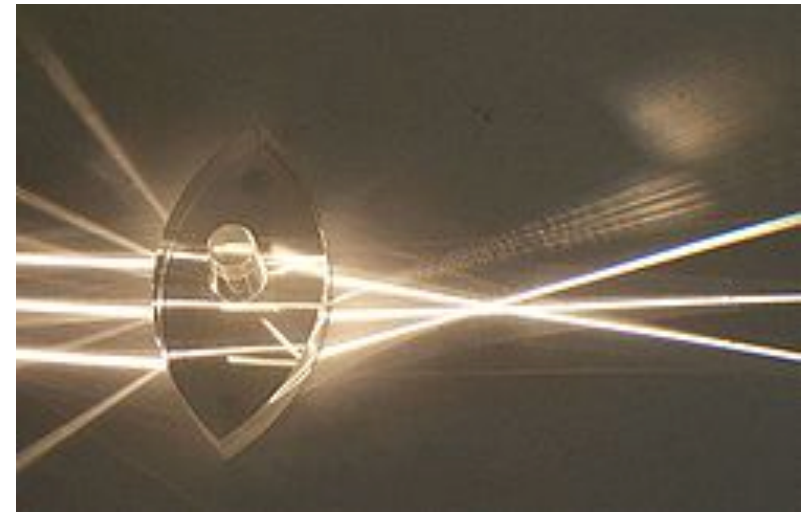
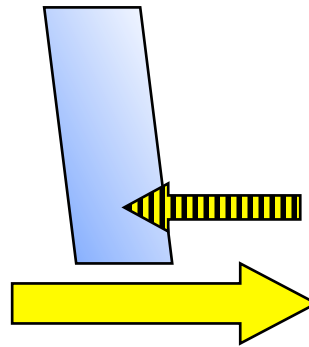
- infinitely long, no changes of properties - no reflection
- can we put at the end of a finite length of TL an impedance such that there are no reflections, in other words, that it looks like an infinitely long TL?

Antenna impedance $\neq Z_0$

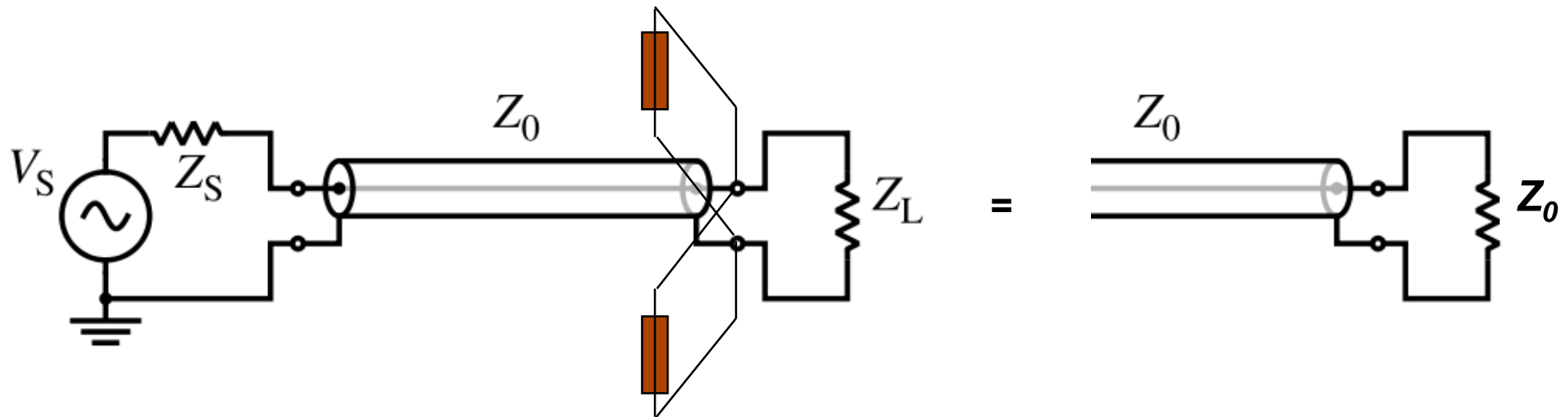


Matching network: two ways to look at it

1) reflect reflections



2) add impedances to match

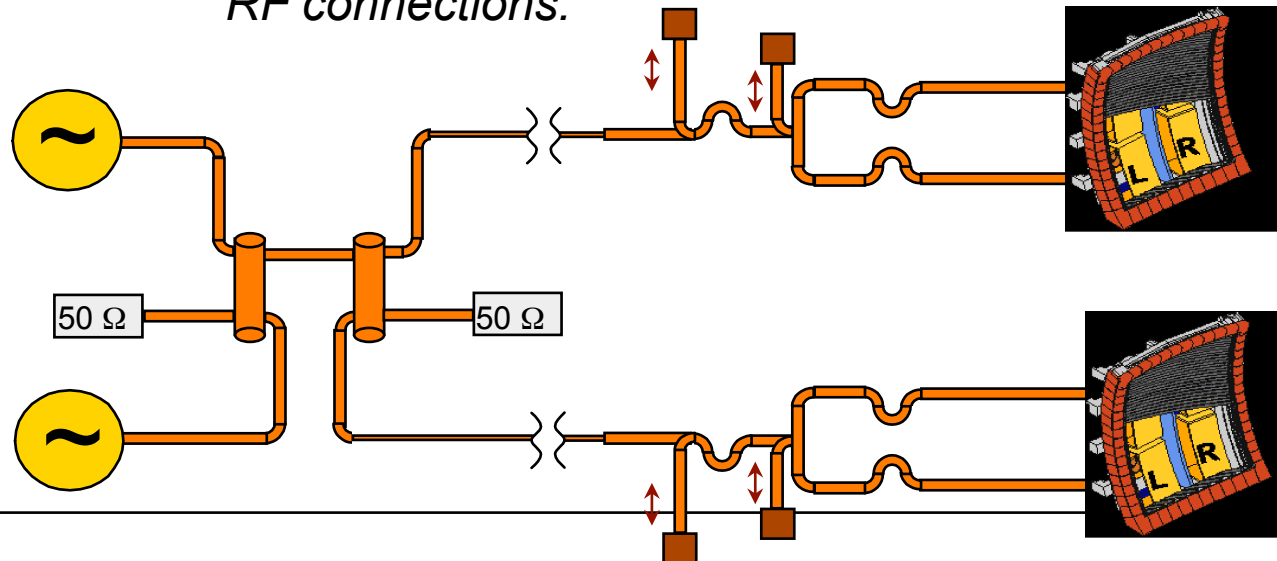


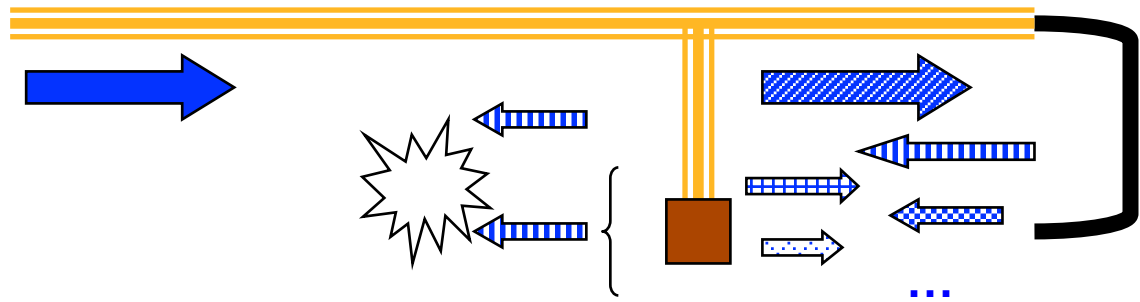
Matching network: reflect reflections



Matching network

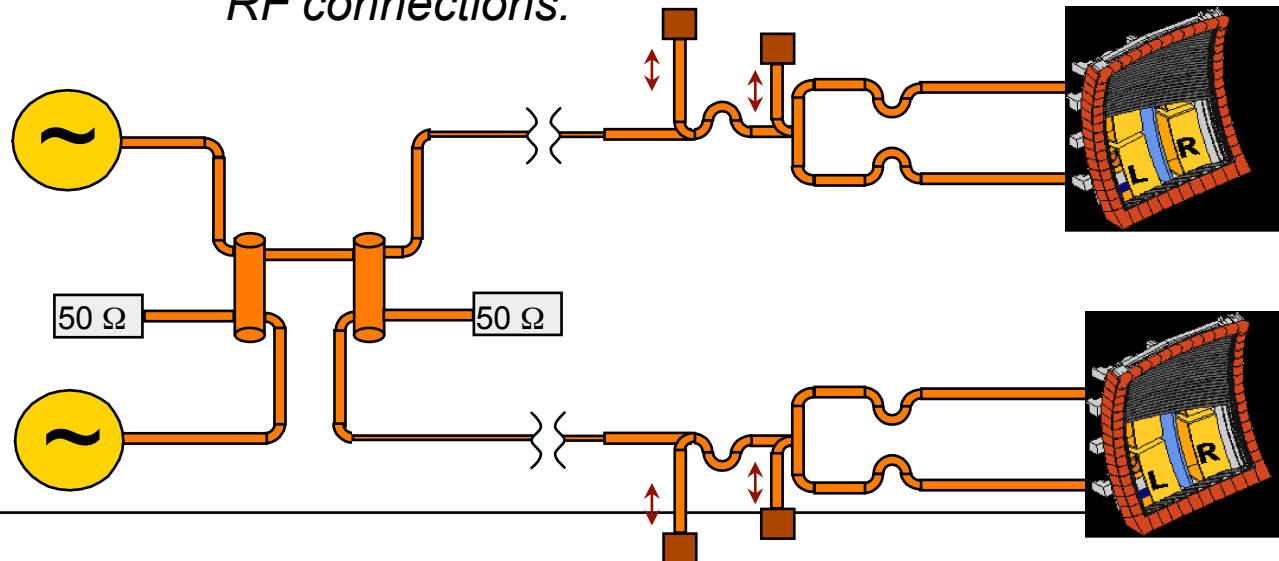
RF connections:



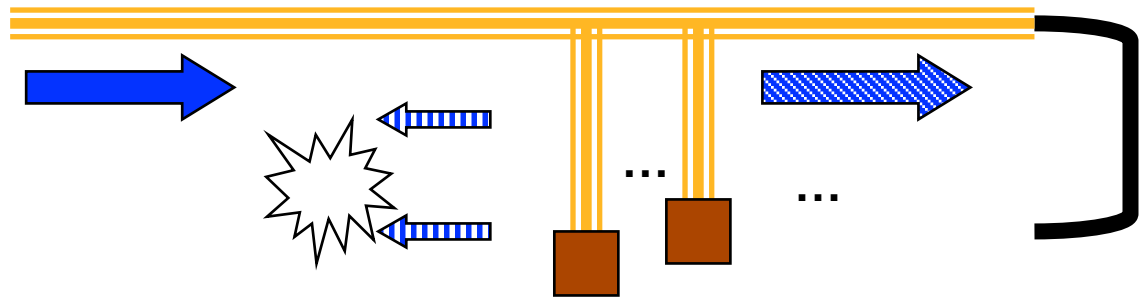


Matching network

RF connections:

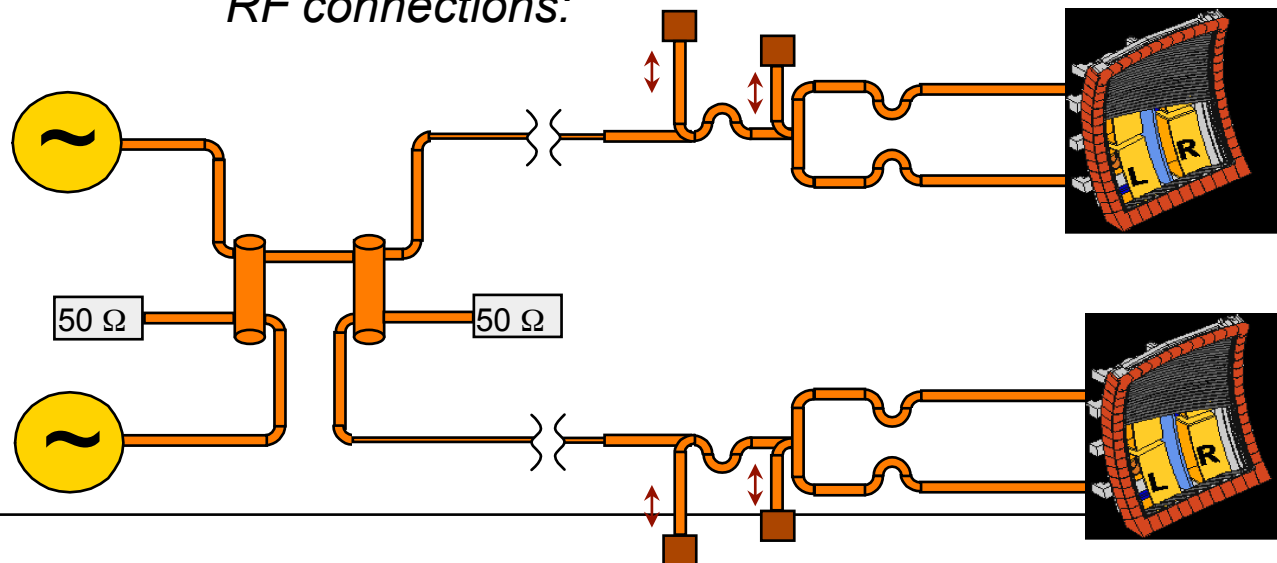


Real and imaginary part

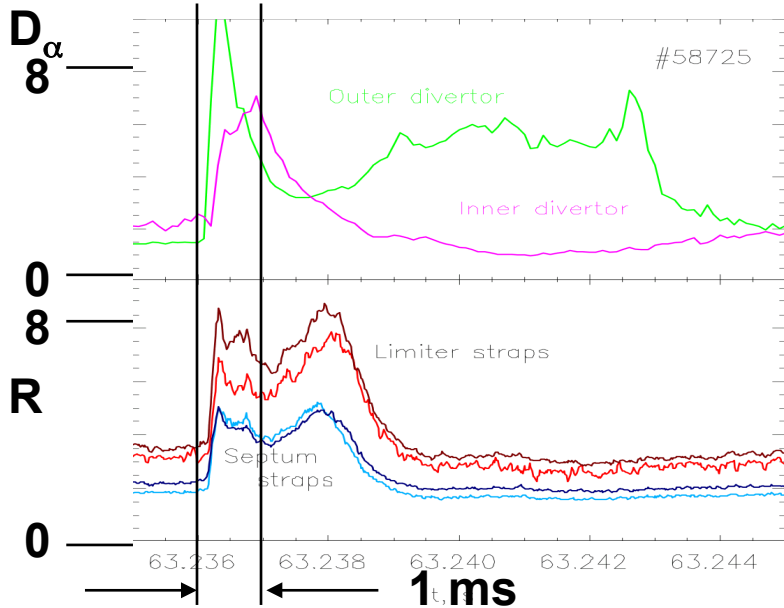
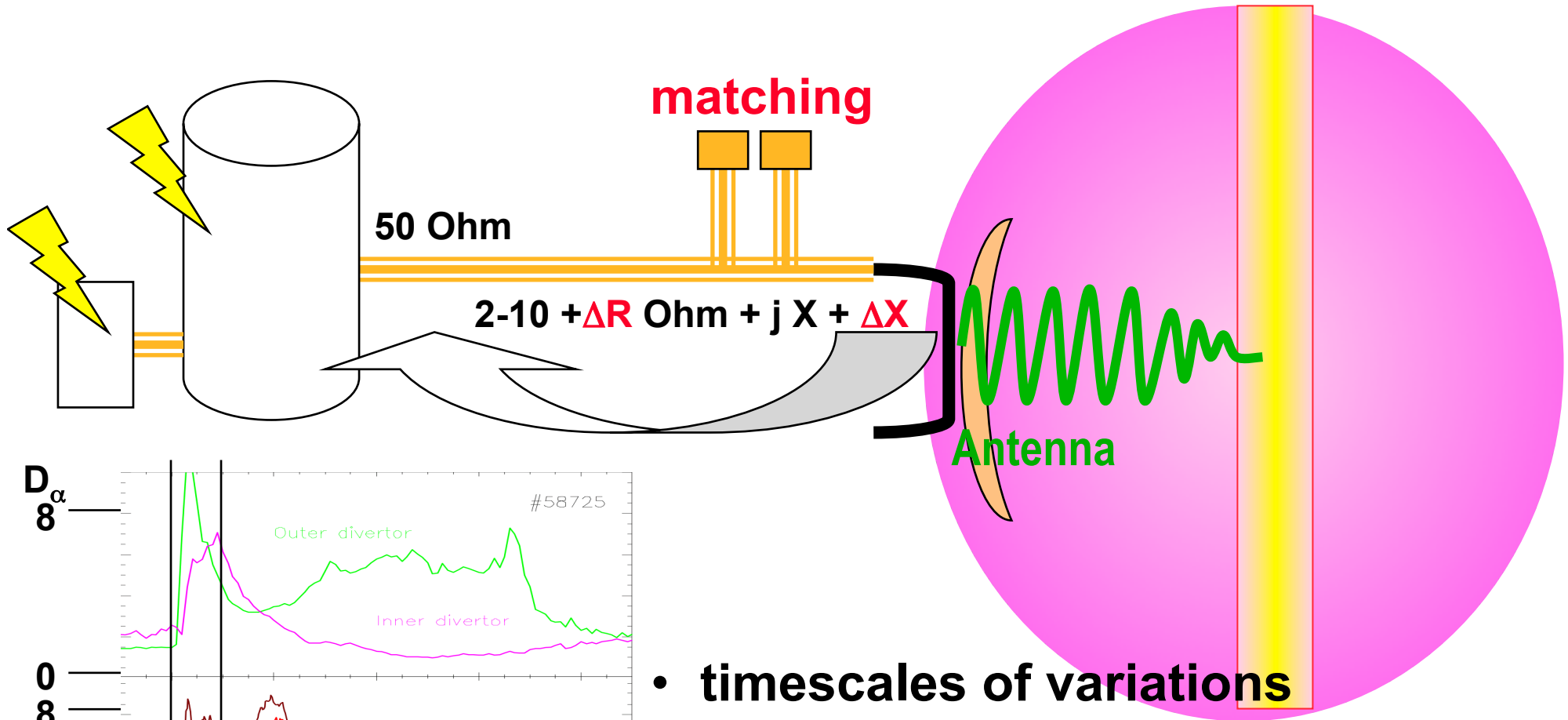


Matching network

RF connections:



Dynamic matching or load isolation necessary

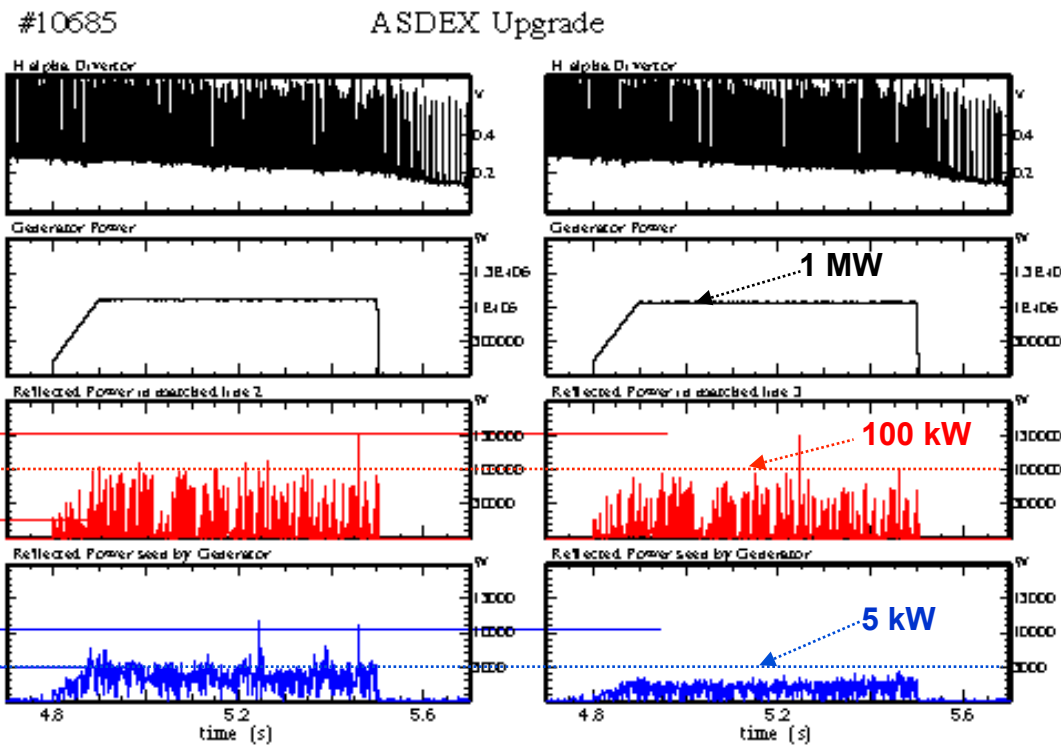
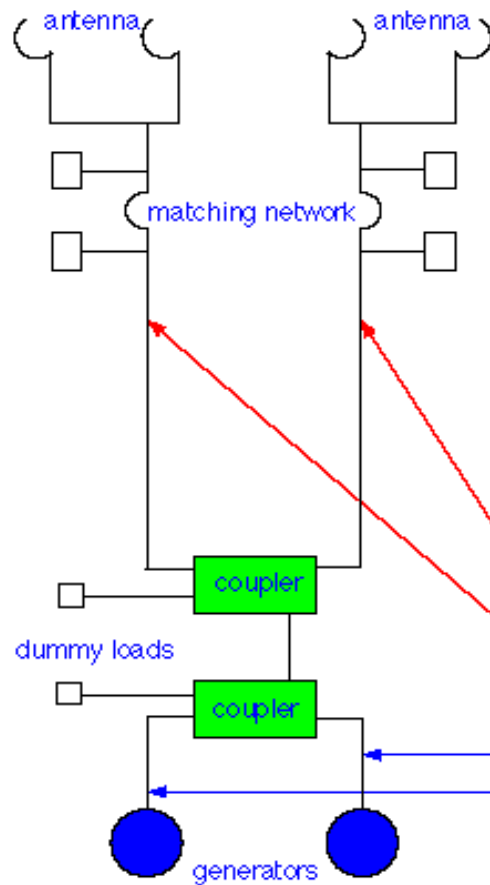


- **timescales of variations**

- particle/energy confinement time ms to s

- MHD events **100 μ s**

3 dB couplers for ELM resilience



H_{α}

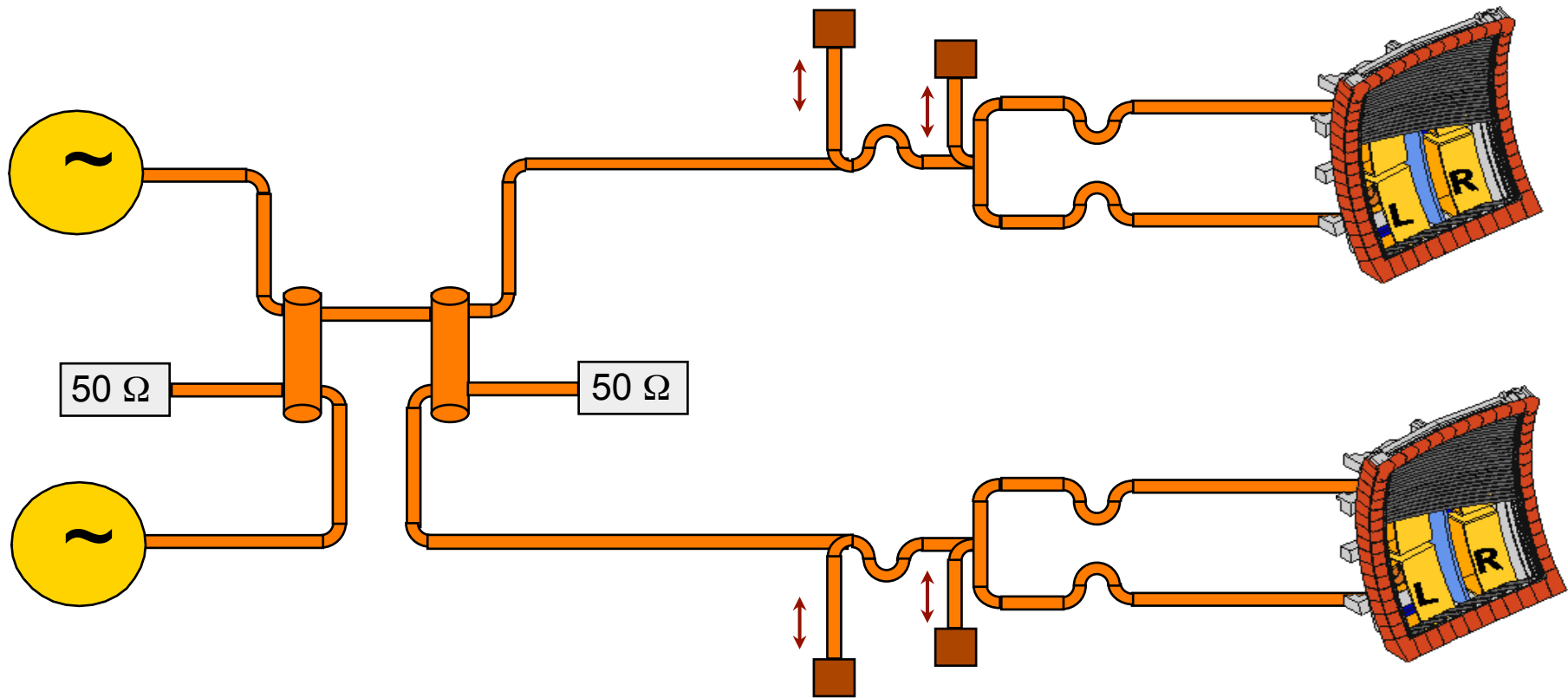
Power to antenna

Reflected power

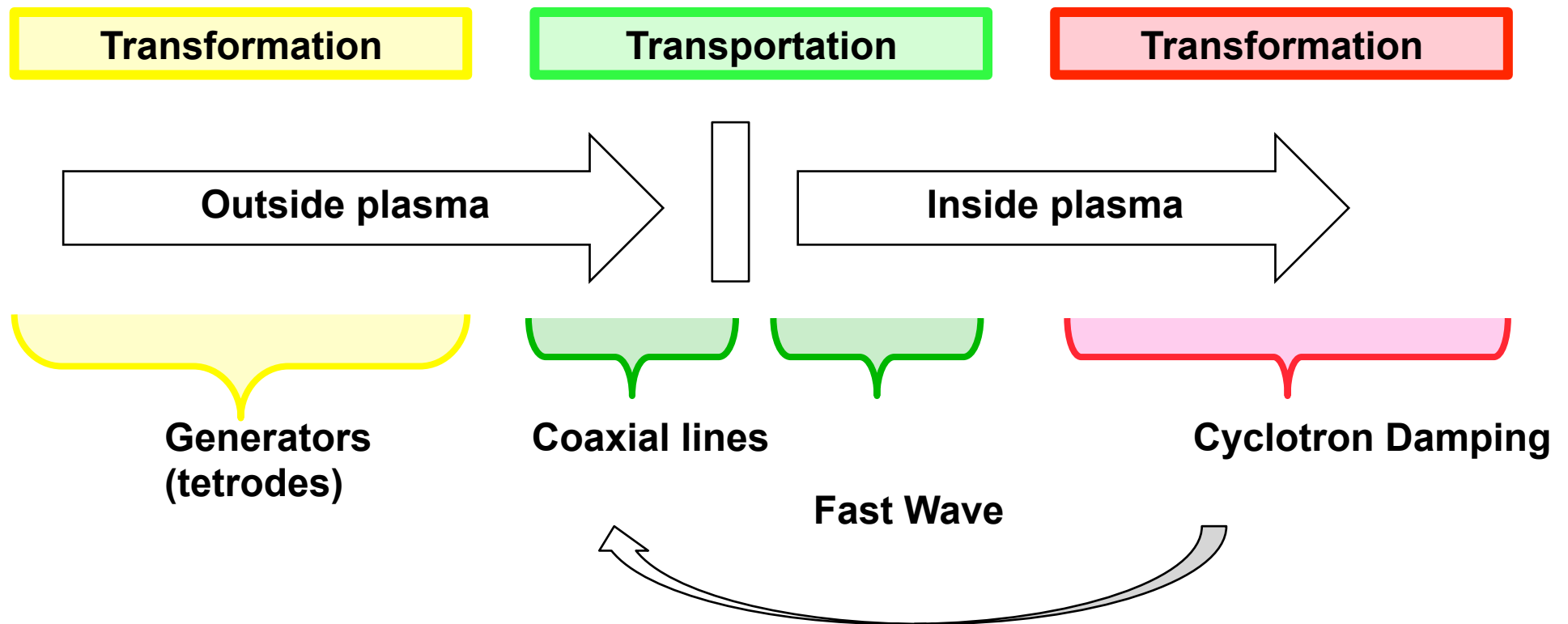
Reflected power at generator

Transmission lines

3 dB couplers and dummy loads



ICRF



Summary EM heating methods



- **for power to be absorbed into the plasma it must first get there**
- **wave propagation: range of frequencies**
 - Electron cyclotron
 - Lower Hybrid
 - Ion cyclotron
- **absorption in plasma: wave - particle interaction**
 - cyclotron damping, also at harmonics
 - Landau damping
- **very large number of possibilities, not just heating**
 - current drive
 - control of instabilities
 - ...

Summary EM heating methods



- **one must also be able to generate and transport the power**
- **Non trivial, examples**
 - **Negative ions**
 - **Gyrotron: high frequency, small dimensions**
 - **LH antenna: PAM**
 - **ICRF: generators and transmission lines**

Remember: 4 steps

Transformation

Transportation

Transformation

Outside plasma

Inside plasma

Electricity -> other form

- fast particles
- electromagnetic oscillations

Transport

(outside part)

(inside part)

- Duct
- optical, waveguides, coaxial and antenna

To plasma particles

- Ionisation
- wave/particle